

Hydrology of Floods Kennebec River Basin Maine Part II

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EXECUTIVE SUMMARY

This report presents Part II of a hydrologic analysis of flooding in the Kennebec River basin. The study was conducted by the Corps of Engineers under the authority contained in Section 22 of the Water Resource Act of 1972. This study was undertaken at the request of the State of Maine.

In September 1985, the Corps of Engineers completed Part I of the investigation entitled "Hydrology of Floods, Kennebec River, Maine." The study reviewed available hydrologic data on floods and analyzed the development and component contributions of recent floods on the river, most notably; December 1973, April 1979, Spring 1983 and June 1984. The document presented here entitled: "Hydrology of Floods, Part II" addressed the effects of storage reservoirs in the basin on Kennebec River flood development.

The Part II study explored the development of reservoir regulation guidance which might further maximize the incidental flood reduction potential of the upper basin storage facilities, without impacting their hydropower function. All season reservoir regulation guide curves were developed by trial through multiyear sequential hydrologic system simulation. Simulations, using the developed guide curves, indicated that greater reservoir storage could be realized with little impact to the downstream flow regime. Storage capacity equivalent to 6 inches of runoff would be available about 65 percent of the time as compared to 40 percent under actual operations. Guide curve operation would likely minimize the spillage during nonspring refill floods, but would not completely prevent spillage during critical spring refill season floods such as the April 1983 and June 1984 floods. When abnormal spring runoff occurs spillage is inevitable. Therefore, secondary guidance was explored in an effort to modify peak discharge rates of spillage when spillage is eminent. Applying the guidance to the experienced April 1979, April 1983 and June 1984 flood events indicated potential reductions of about 30 percent in peak rates of spillage.

A review of surcharge storage characteristics at the three major storage reservoirs revealed no opportunities for any significant added use of surcharge storage for flood control purposes.

A cursory analysis was made of the relative effectiveness of any new flood control storage in various presently uncontrolled subwatersheds upstream of Waterville, Maine. Resulting average main stem flood stage reduction per 100,000 acre-feet of storage varied from about 1.0 to 2.5 feet for different subwatersheds with the maximum effectiveness indicated for the Carrabassett tributary. A component contribution analysis of the recent major Kennebec River flood of March/April 1987 demonstrated the

flood producing potential of runoff from the uncontrolled downstream watersheds. This spring flood was the flood of record generally throughout the mid to lower Kennebec basin and occurring with upper basin reservoirs controlling the runoff from their contributing watersheds. Had it not been for the availability of upper basin reservoir storage, the devastating flood of 1987 would have been considerably worse.

In summary, the Part I and II reports provide hydrologic information, analysis, and guidance in the interest of facilitating a common understanding for planning and designing flood damage reduction projects and programs. The study revealed two flood reduction opportunities on the main stem of the Kennebec River. The adoption of monthly guide curves for the major storage reservoirs in the upper basin could reduce the effective runoff contribution from these watersheds. In the uncontrolled watersheds above Waterville, Maine, potential flood stage reduction could be achieved through the development of additional flood control storage. The amount of flood stage reduction is dependent upon the location of the storage facility.

This study was performed under the Corps of Engineers' Section 22 Program administered by Messrs. John R. Kennelly and John E. Kennedy of the Corps of Engineers, Planning Division, under the direction of Mr. Joseph L. Ignazio. The hydrologic investigation was completed by Messrs. Philip Manley and Mark Gieb of the Hydrologic Engineering Section under the direction of Mr. Richard D. Reardon.

HYDROLOGIC ANALYSIS OF FLOODS
KENNEBEC RIVER
MAINE

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HYDROLOGIC ANALYSIS OF FLOODS
KENNEBEC RIVER, MAINE
PART II

1. PURPOSE

This Part II report, on the "Hydrologic Analysis of Floods" in the Kennebec River, presents:

a. The results of exploratory system simulation studies in search of reservoir regulation guidance that might maximize the incidental flood control effectiveness of upper basin reservoirs while not impacting their design purpose, i.e., hydropower storage.

b. Information on the relative flood control effectiveness if new reservoir storage were provided in various uncontrolled tributary watersheds.

c. An assessment of the potential for added flood control surcharge storage at the existing upper basin reservoirs.

These issues were studied, at the request of the Maine State Planning Office, as a continuation of the original (Part I) 1985 study report. Also included in this report is a summary hydrologic analysis of the recent major March/April Kennebec River flood.

2. BACKGROUND

In September 1985, the Corps of Engineers completed a study report entitled: "Hydrology of Floods, Kennebec River, Maine." The study was performed for the Maine State Planning Office under authority contained in Section 22 of the Water Resources Development Act (PL 93-251) of 1974. Included in the earlier report were sections on basin description, climatology, streamflow and flood history. Its purpose was to review available hydrologic data on floods and analyze the development, and component contributions, of recent floods on the river, most notably: December 1973, April 1979, April 1983 and June 1984.

As a followup to this earlier report, the State requested Part II studies exploring (a) seasonal "guide curves" for regulating the large headwater storage reservoirs (Brassua, Moosehead and Flagstaff), in the interest of possibly enhancing incidental flood control and, (b) the relative effectiveness if new flood control storage were built on

selected uncontrolled tributaries, as well as the potential of surcharge storage use at existing reservoirs.

A map of the Kennebec River basin is shown on plate 1. Principal tributaries and existing reservoir storages are listed in tables I and II.

TABLE I
KENNEBEC RIVER
PRINCIPAL TRIBUTARIES

<u>Tributary</u>	<u>Drainage Area (sq.mi.)*</u>	<u>Length (miles)</u>	<u>Fall (feet)</u>
Moose River	722	76	750
Dead River	874	23	570
Carrabassett River	401	35	636
Sandy River	596	69	1544
Sebasticook River	946	48	270

* U.S. Geological Survey, Open File Report,
"Drainage Areas of Rivers and Streams in
the Kennebec River Basin," September 1980.

3. RESERVOIR GUIDE CURVES

a. General. Ten hydroelectric dams on the main stem of the Kennebec River make up 95 percent of the total hydropower generating capacity in the Kennebec basin. All the main stem dams are "run-of-river" except Harris (Indian Pond) and Wyman which have storage capacity only for daily or weekly load fitting operations. Principal storage reservoirs in the basin are in the headwaters above Bingham and are used for hydropower regulation. There are 1,132,000 acre-feet of storage in the basin and 1,016,500 acre-feet, or 90 percent, are at the three lakes: Brassua, Moosehead and Flagstaff.

Storage reservoirs are used in hydropower operations to store excess waters during high flow periods for later release and use during low flow periods, thereby, ensuring a

TABLE II
AVAILABLE RESERVOIR STORAGE*
KENNEBEC RIVER BASIN ABOVE BINGHAM, MAINE

<u>Project</u>	<u>Drainage Area (sq.mi.)**</u>	<u>Surface Area (acres)</u>	<u>Drawdown (feet)</u>	<u>Storage (ac-ft)</u>	<u>Percent</u>
Brassua Lake	716	8,979	30	196,500	17
First Roach Pond	70	3,270	7	21,500	2
Moosehead Lake	1,268	74,000	7.5	544,000	48
Indian Pond (Harris)	1,384	3,747	5	19,000	2
Moxie Pond	80	1,747	8	14,700	2
Flagstaff Lake	516	17,950	35	276,000	24
Wyman Lake	2,619	3,145	20	<u>60,300</u>	<u>5</u>
				1,132,000	100

* Storage Data from U.S. Geological Survey Water Data Report ME-83-1

** From U.S. Geological Survey, Open File Report, "Drainage Areas of Rivers and Streams in the Kennebec River Basin," September 1980

minimum dependable hydropower generation. From a hydropower perspective, water in storage is "money in the bank" and releases in excess of hydropower capacity, are "spillage" or "wastage" and represent revenue lost.

Therefore, reservoir regulation for hydropower generally involves trying to maintain sufficient water in storage to provide hydropower dependability while at the same time maintaining storage space in anticipation of excess runoff. Because of limited storage capacity the majority of hydropower reservoirs are used as "pondage" primarily for daily or weekly "load fitting" operations. It is only the real large storages such as Brassua, Moosehead, and Flagstaff that are of such size as to permit seasonal storage regulation. These storages are generally filled each spring during the snowmelt high flow season and then drawn down during the following summer, fall and winter seasons. The three Kennebec headwater storages are operated as a system to provide a lower main stem flow for hydropower.

Hydropower storage reservoirs, with no design storage for flood control, cannot ensure floodflow reductions during all floods; however, during periods when storage is drawn down for hydropower, their ability to store storm runoff does provide a degree of incidental flood control. The degree of such incidental flood control benefit is a function of the percent of time, and amount, the reservoir is drawn down in its hydropower operation. Such incidental flood control benefits are real if the reduced frequency of flooding does not create public complacency on the part of downstream flood plain occupants, resulting in more flood plain development and thus increased flood damages when the less frequent but unmodified floods do occur. Therefore, appropriate flood plain zoning is a vital feature of any water resource management plan involving incidental flood control by nonflood control reservoirs.

The purpose of the study, reported herein, was to explore the development of reservoir regulation "guide curves" that might tend to maximize the incidental flood control provided by the three upper basin reservoirs, while at the same time not impact on their hydropower function. The exploration studies were facilitated by computer hydrologic system simulations.

b. Procedure. In summary, the study procedure was as follows: the three-reservoir system operation was first simulated for a historical hydrologic period of years to determine the minimum dependable yield of the system during critical drought periods. Secondly, having established the

minimum dependable yield and knowing the average system yield, a series of trial simulations were made to establish monthly target release rates, as a function of amount of water in storage (guide curves), that would tend to: (1) maximize regulated flows during normal periods, (2) minimize spillage and wastage during wet periods, and (3) still maintain sufficient water in storage to meet minimum dependable yield during critical drought periods. Striving to meet the above goals would tend to maximize hydropower capability but also maximize incidental flood control storage availability. All system simulations were performed with the aid of the Corps of Engineers computer program HEC-5, "Simulation of Flood Control and Conservation Systems," using a monthly time increment. Streamflow data (system inflow) was determined using the published flow data for the Kennebec River at the Bingham, Maine U.S. Geological Survey gage and adjusting for monthly change in upstream reservoir contents. This computed monthly flow data was then prorated by respective drainage area size to determine monthly reservoir inflows and contributions from uncontrolled local areas. The system was first simulated for the period 1951 to 1984 (34 years) to establish minimum yield. The period 1955 to 1975 (21 years) was then selected as a representative hydrologic period and used as the test period for the numerous subsequent trial simulations.

Though the three reservoir system is operated for a series of main stem hydropower plants, for these simulations the reservoirs were operated for a single main stem index point, that being the Bingham USGS gage site located a short distance downstream of the second largest hydropower project on the Kennebec: Wyman Dam. All hydrologic simulation and guide curve development studies were intentionally made completely independent of any existing or historical operational trends or procedures, thereby, avoiding any prestudy bias or preconceived operational criteria.

Brassua and Moosehead Lakes are two reservoirs in tandem and they operate in parallel with Flagstaff Lake in providing flows to Wyman and other downstream hydropower plants. As previously stated, the three-reservoir system, plus the intervening uncontrolled local, was operated for the Bingham gage as the single downstream index control point. Operating criteria for individual reservoirs was selected to maintain the three storages generally in balance with respect to percentage of total usable storage capacity. The only exception was that when first initiating drafting from full reservoirs, drafting, from Moosehead would precede drawing from Brassua, thus minimizing the possibility of drafting at Brassua while spilling at Moosehead. Similarly, at the lower extreme of

storage utilization, Brassua would be emptied before Moosehead to try and avoid Moosehead not being able to meet downstream control flow while there was still water in storage at Brassua.

Guide curves, both monthly and seasonally, were developed by trial simulations and by analysis of average and drought runoff periods. The monthly "guide curves" took the following form. Each month there was an established target flow at Bingham. If total system water in storage was within limits established for the specified month then the system was operated to meet the target flow. If for any month the total system storage fell below the established lower limit, the system would operate for a lower limit minimum flow at Bingham. Similarly, if system storage exceeded the upper limit, the system was operated for an upper limit flow at Bingham. Obviously, in the event inflows minus requested outflows exceeded available storage at any of the three reservoirs, then all excess inflows, above storage capacity, were released downstream.

It is noted that with the simulation used, there were three control flow conditions for each month, either desired flow, minimum flow, or maximum flow. It would be expected that, in an actual day-to-day operation, transitional rather than stepped guide curves would be used to relate control flow versus total system storage.

c. Results. The resulting monthly "guide curves" of Bingham target flow versus total system storage, developed by trial, are shown on plate 2. The simulation studies demonstrated, as is commonly known, that storage refill is generally during the spring runoff period (April to May). Draw-down can commence generally in July and continue throughout the year to the beginning of the subsequent spring refill period. The degree to which storage can be filled in the spring determines the project's ability to ensure a minimum dependable flow throughout the coming year. Progressing through the year, the length of time to the next refill becomes less; therefore, the amount of reserve storage required becomes progressively less. By simulation of several years, sequentially, the monthly minimum storage levels are established which would necessitate going to minimum flow, but, equally important, upper limits are established indicating likely excess of storage to meet normal flow. Excess storage can be released for downstream use, which may reduce later spillage (wastage) during high flow. It is the use and orderly release of excess seasonal storage that would tend to maximize incidental flood control.

As the guide curves indicate, the minimum dependable yield of the system at the index point, Bingham, was found to be about 2,000 cfs, with a normal capability of about 4,000 cfs. The guide curves were developed with an all season minimum required target flow of 2,000 cfs, and all season desired target flow of 4,000 cfs except April. Following a series of simulations, the desired target flow for April was increased to 8,000 cfs in trying to reduce the frequency and magnitude of spillage from filled storages during spring runoff. Maximum target flow was set at 6,000 cfs from June through February with 8,000 for March, 10,000 for April and 8,000 for May.

It is noted that these upper limit release rates are in excess of the hydropower capacity of many of the main stem projects. Maximum capacity in the system is at Wyman, at about 9,000 cfs. The guide curves simply indicate that, at times, the system can provide these higher flows without impacting on later required flow capability and possibly reducing later spillage rates from the storages. The readers of this report should keep in mind that the storage reservoirs are owned and operated for hydropower. From a hydropower perspective there could rightfully be hesitancy at making regulated releases from storage, in excess of hydropower capacity, to minimize the chance of later spillage from storage during a flood period. Hydropower interests might view any flow in excess of hydropower capacity as "wastage" whether it be as a result of spillage from storage during a flood or regulated releases in excess of hydropower capacity.

Upon completion of the system studies, reported herein, a meeting was held on 29 June 1987, with Mr. Corson of the Kennebec Water Power Company, the operator of the three upstream storage reservoirs for downstream owner-clients. The purpose of the meeting was to discuss the studies and inquire of existing operating procedures, criteria and restraints. His plan of operation in general is to maintain a target flow of 3,600 cfs at Madison and then vary up or down from a minimum of about 2,000 cfs to a maximum of about 4,500 cfs, depending on total system storage for the particular month relative to normal storage, as determined from the mean of several years of operation. (Madison is about 25 river miles downstream of Bingham with about 460 square miles of intervening drainage area). He indicated that he had been attempting to draft more in late winter the last few years and relying on spring snowmelt runoff for ample storage refill. He meets at least once a month with the five owner clients regarding operational plans for the next month and he noted that final decisions and recommendations on operation are usually based on

varying factors within general guidelines rather than in accordance with any hard rules. Other considerations, though not hard rules or restraints, were that the Fish and Wildlife Service preferred that Moosehead levels not fall below the 10 to 15 October level and that recreational interests would be disturbed if lake levels were significantly below normal during the summer season.

Following development of the seasonal guide curves the results of simulations, using the curves, were compared with actual historic operations. Monthly system operations, both observed and as simulated, for the test period 1955 to 1975 are compared graphically on plates 3 and 4. A computer input-output of an HEC-5 Guide Curve Simulation is appended to this report. Summary plots of average monthly flows at Bingham and system storages, observed and as simulated, are shown on plates 5 and 6. Comparative Bingham flow durations (flow versus percent time) and system storage duration curves are shown on plates 7 and 8.

The bottom line result was that the Bingham flow regime, by guide curve simulation, was remarkably similar to the actual historical flow regime as recorded and published by the U.S. Geological Survey for the Kennebec River at Bingham. On average the simulation indicated about a 20 percent increase in average April flows with a subsequent reduction of about 10 percent for the peak flow month of May (reference plate 5). Simulated flows averaged about 10 percent higher in October and November while about 15 percent lower in February and March. Other months the average flows were nearly identical. Though the flow regime was not markedly different than observed, reservoir storages with the simulation were consistently lower than actual for the historical period (reference plate 6). This is attributed largely to the guide curves calling for increased releases during wetter than normal periods. Simulated storages averaged about 100,000 acre-feet, about 10 percent of total system storage, during the summer season. This 10 percent would represent about 0.7 foot difference in lake level at Moosehead Lake, which might impact recreation. The lower levels of storage resulted in some reduction in (but did not eliminate) spillage during high runoff periods. Most noticeable was the effect during nonspring runoff periods. For example, the December 1973 flood event (water year 1974) resulted from intense rainfall occurring with reservoirs high as a result of an above average runoff summer. The guide curve simulation indicated that the reservoirs would have been drafted sufficiently to store the flood runoff with the maximum monthly control flow at Bingham 6,000 cfs. It is believed that another earlier similar December flood event occurred in 1901.

The monthly guide curve simulations indicated a reduced probability of storage spillage during nonspring refill seasons; however, floods most frequently occur during, or just following, the spring runoff (March 1936, March 1953, April 1979, April 1983 and June 1984) and the guide curve operation was not nearly as effective in eliminating spillage during the spring refill. The guide curves must permit spring storage refill from normal spring runoff; therefore, events that produce abnormally high spring runoff usually result in required spillage at the storage reservoirs and potential for significant contributions to downstream flood flows. Average spring runoff during April and May in the upper Kennebec Basin is about 11 inches or about 46 percent of total annual runoff. Also the April and May runoff can range as high as 17 inches. Total usable storage in the three reservoir system is equivalent to about 10 inches of runoff from their respective watersheds. The total capacity is not available for storage each spring because of the need to retain some water in reserve for unpredictable events such as abnormally low or late spring runoff. Reportedly the lower approximate 1 foot of storage at Moosehead Lake is usually retained both as reserve and due to discharge limitations at the lake outlet.

Because of the high flood sensitivity during the spring season and the limited capability of monthly guide curves to regulate the limited storage for short duration abnormally high runoff events, further exploratory studies were made of potential guide curves for spring refill regulation, using a daily rather than monthly time increment.

d. Spring Refill Guide Curves. The greatest potential for filling and spillage at the upstream storage reservoirs is during the spring refill-runoff period, April, May and June. Greatest spillage contributions to downstream flooding occurs when significant rainfall or snowmelt runoff occurs with the storages initially at, or near, full. Therefore, spring refilling guide curves using a daily time increment, were explored in the interest of minimizing the probability of premature filling of the lakes during the April - May refill period. Any such guide curves would also require that they not increase the probability of not refilling the lakes during drought years. The guide curves were developed by analyzing mean, maximum and minimum lake inflow rates, for the 2-month period April and May, and developing, by trial, total system storage level versus suggested target regulated flow rates at Bingham, to accomplish orderly filling of system storage.

The developed exploratory guide curves are shown on plate 9. In applying the guide curves to experienced high

flow events it was found impossible to prevent spillage in most instances; therefore, secondary guidance was explored on project operations during pending flood situations that might modify the peak rate of spillage when spillage was imminent. For example, if storage levels were high and the system was being operated for a target flow at Bingham, in the event of a high runoff occurrence there could be a tendency to cut back releases at the reservoirs, resulting in accelerated filling and later magnified spillage contributing to downstream floods. Secondary guidance was therefore added to the spring refill guide curves that would attempt to modify peak spillage when spillage was imminent. This was accomplished by calling for higher controlled releases from the reservoirs, when storage levels were high, thereby reducing the magnitude of subsequent spillage. The secondary guidance added to the spring guide curves was as follows:

(1) Total System Storage Less Than 900,000 Acre-Feet

(a) Typical Condition. If the guide curve target flow at Bingham is less than 12K and total system storage is less than 900,000 acre-feet (90 percent full) then reservoirs would be operated for the indicated target flow, even to the point of near zero outflow.

(b) Moderate High Storage Early in Season. If the target flow at Bingham is between 12 and 14K and total storage is less than 900,000 acre-feet, reservoirs would be regulated for the 12K target flow but combined outflows would not be made less than 8K.

(c) High Storage Early in Season. If target flow is greater than 14K and storage is less than 900,000 acre-feet, regulation would be for the 14K at Bingham but combined outflows would not be less than 10K.

(2) Total System Storage Greater Than 900,000 Acre-Feet

(a) Typical in Late Spring. If target Q at Bingham is less than 12K but total storage is greater than 900,000 acre-feet then minimum storage outflow would be for target flow or made equal to one-half of the computed rate of inflow to storage, whichever is greater.

(b) Moderate High Storage in Late Spring. If target Q is between 12 and 14K minimum regulated outflow would be 8K or one-half inflow whichever is greater.

(c) High Storage in Late Spring. If target Q is greater than 14K and total storage greater than 900,000

acre-feet, then minimum outflow would be 10K or one-half of inflow, whichever is greater.

The developed spring refill guide curve, shown on plate 9, in concert with the above secondary guidance was tried with the recent spring floods of April 1979, April 1983 and June 1984. As stated earlier, use of the monthly guide curves indicated that there would be no spillage under conditions of a December 1973 flood.

Experienced storage levels at the start of spring refill (1 April) were higher than those resulting with the monthly guide curve simulation; therefore, the spring guide curves were tested under the more severe historical starting (1 April) storage. The results of the three trial floods are summarized in table III. Results indicated that use of the spring guide curves might have reduced peak flow at Bingham from about 40,000 to about 29,000 in April 1979 (27 percent), from about 55,000 to about 47,000 in April 1983 (14 percent) and from about 65,000 to 53,000 cfs (18 percent) in June 1984.

All trials were performed combining all three storages and computing inflow to storage by drainage area ratio with the recorded unregulated Carrabassett riverflows. The unregulated local contribution downstream of the storages above Bingham was also estimated by ratio of drainage area and mean annual runoff with the Carrabassett flows. The resulting regulated outflows from storage using the guide curves were compared with the experienced outflows (reference 1985 report) in determining peak discharge reductions. All trials were also made allowing for no surcharge storage above assumed full system storage capacity of 1 million acre-feet.

Secondly, the spring refill guide curves were tested under the severe droughts of April to May 1957 and 1965 to determine if there would be impact on ability to refill storage sufficient to ensure minimum dependable flow. Since the Monthly Guide Curve Simulation had demonstrated ability to meet the minimum dependable target flow at Bingham, the amount of April to May storage drought refill, using the Daily Spring Refill Guide Curves, was compared with the refill indicated by the monthly simulation. In both test droughts the daily guide curves resulted in April to May refill in excess of that with the monthly curves. However, in both cases the system storage levels were considerably less than experienced. Comparative storage data for the droughts of 1957 and 1965 are shown in table IV. Regarding the developed Guide Curves, the operator of the reservoirs has noted that present hydrologic instrumentation, data transmission

TABLE III
RESERVOIR OPERATION
DURING SPRING REFILL FLOODS
COMPARATIVE DATA

	<u>April 1979</u>	<u>April 1983</u>	<u>June 1984</u>
<u>MOOSEHEAD-FLAGSTAFF</u>			
Peak Discharge			
As Experienced	18,000± cfs	26,000± cfs	34,000 cfs
With Guide Curves	12,000	17,000	27,000
Δ	6,000	9,000	7,000
%	-33%	-34%	-20%
Peak Contribution to Bingham Flood			
As Experienced	11,000± cfs*	16,000± cfs*	32,000 cfs
With Guide Curves	0	8,000	20,000
Δ	11,000	8,000	12,000
%	-100	-50	-37
Δ Stage	-1.5± feet	-1.1± feet	-1.7± feet

* Contribution to First Peak

TABLE IV
RESERVOIR SYSTEM OPERATION
DURING SPRING REFILL DROUGHTS
COMPARATIVE DATA

	<u>April-May 1957</u>	<u>April-May 1965</u>
<u>WATER IN STORAGE (Acre-Feet)</u>		
Starting/Ending		
Experienced	147,310/659,960	209,550/650,290
With Monthly Guide Curve	40,660/360,410	60,000/384,260
With Daily Guide Curve	40,660/441,430	60,000/540,740
<u>CHANGE IN STORAGE (Acre-Feet)</u>		
Experienced	512,650	440,740
With Monthly Guide Curve	319,750	324,260
With Daily Guide Curve	400,770	480,740
<u>MINIMUM FLOW AT BINGHAM (CFS)</u>		
Experienced	1,330*	1,340*
With Monthly Guide Curve	2,000	2,000
With Daily Guide Curve	2,000	2,000

* Minimum experienced daily flow likely
 effected by regulation at Wyman

and weather forecasts in the basin, during high runoff periods, are inadequate to permit operating for a target flow at a downstream location and releases during high runoff were generally based on storage conditions at the reservoirs. He also noted that the mode of operation at the reservoirs was not conducive for making frequent changes in release rates, particularly any operation calling for night time gate changes where personnel safety could be at risk.

4. FLOOD STORAGE EFFECTIVENESS

This section presents data and discussion on the estimated magnitude of flood stage reductions that might be provided by flood control storage on selected uncontrolled tributaries and central basin intervening local areas. In the earlier 1985 Flood Hydrology study it was concluded that the Sandy and Carrabassett Rivers were large contributors, relative to watershed size, to lower main stem Kennebec River floodflows. For the four floods reviewed, i.e., December 1973, April 1979, April 1983 and June 1984, the contributions from the Sandy and Carrabassett Rivers to peaks on the lower main stem averaged an estimated 30 percent of floodflow. In the more recent 1987 flood the percent contribution from these two streams was even greater (more nearly 40 percent) because of the negligible contribution from the upper basin storage reservoirs.

In the current analysis, the Carrabassett and Sandy River component flood contributions were compared with four other central basin uncontrolled component local watershed areas. Component contributions, in percent of total, to lower main stem floodflows for the six areas are listed in table V along with their respective drainage areas. Also listed are average component contributions to flood stages in feet, which were based on the U.S. Geological Survey stage-discharge rating for the gage at North Sidney. All component contributions were based on the average for the four floods previously referenced, and does not include the latest 1987 flood which would skew the contributions somewhat higher due to the lower upper basin contributions.

Next, the estimated average potential flood stage reduction in feet was computed per 10,000 acre-feet of flood control storage in each of the respective component watersheds. Flood control needs per square mile of watershed were based on a minimum storage capability of 6 inches of runoff which is equivalent to about 318 acre-feet of storage per square mile of watershed controlled. This last step of the analysis provided quantitative information on flood stage reduction per unit storage, and also relative effectiveness of storage

among the six component watersheds. For example, the flood stage reduction per unit of storage in the Sandy and Carra-bassett Basins was about double that of some of the other component areas. A summary listing of results is presented in table V. No attempt was made to locate potential flood control storage sites in any of the component watersheds and thus no comparative information has been developed on cost per unit of storage in the different areas.

5. SURCHARGE STORAGE

a. General. Surcharge storage in a reservoir is generally defined as that storage volume between the crest of an uncontrolled spillway (or between the normal full pool elevation of a gated spillway with the crest gates in the normal closed position), and the maximum water surface for which the dam was designed to withstand. Maximum design water surface generally equals top of dam elevation minus a design freeboard, and often represents maximum pool levels under spillway design flood conditions. A cursory review of the surcharge storage characteristics of the three storage reservoirs: Brassua, Moosehead and Flagstaff, revealed no opportunity for any significant use of surcharge storage for added flood control regulation.

b. Brassua Lake. This project has a usable storage capacity of about 9.0 billion cubic feet (200,000 acre-feet) between a minimum pool elevation of 1043 and a maximum normal full pool elevation 1074 feet NGVD. With a surface area of about 9,000 acres and a watershed area of 716 square miles, each foot of surcharge over elevation 1074 would represent 9,000 acre-feet, equivalent to only about 0.25 inch of runoff from its watershed. Therefore, it was concluded that several feet of surcharge storage would be needed at Brassua to provide any significant additional flood control storage.

Flows from Brassua are regulated with four 6-foot diameter low level sluices (sill elevation 1034), a gated log sluice (sill elevation 1057), and fifteen 15-foot wide stop-logged sections between elevations 1065 and 1074 feet NGVD. Top elevation of the earth embankment section of the dam is 1081.5 and the concrete nonoverflow section is 1079.5 feet NGVD. In the past the owners have proposed raising the normal full pool at Brassua, by adding stoplogs, from elevation 1074 to 1076, providing about 18,000 additional acre-feet of usable storage; however, this proposal is still pending. With projects having gated spillways an amount of surcharge storage is required above normal full pool to allow time for gate operation and for the establishment of gate operating schedules based on surcharge pool level and rate of

TABLE V
KENNEBEC RIVER BASIN
COMPONENT CONTRIBUTIONS TO FLOODFLOWS
AND
FLOOD STORAGE EFFECTIVENESS

<u>Component</u>	<u>Drainage Area (sq.mi.)</u>	<u>Average % Con- tribution to Lower Main Stem Floodflows (percent)</u>	<u>Average Flood Stage Contribu- tion to Lower Main Stem Floods (feet)</u>	<u>Flood Stage Reduc- tion per 10,000 Acre-Feet of Flood Storage* (feet)</u>
Kennebec River Local Above Forks	322	8.76	1.7	0.16
Dead River Local	358	5.55	1.1	0.097
15 Forks to Bingham Local	251	8.33	1.6	0.20
Carrabassett River	354	14.31	2.7	0.24
Sandy River	514	16.45	3.1	0.19
Sandy to Waterville Local	538	9.18	1.8	0.10

* Flood storage based on minimum of 6 inches (318 acre-feet) per square mile of watershed controlled

rise. It was concluded that there was no opportunity for surcharge storage regulation at Brassua Lake, beyond the incidental flood control provided by existing gate regulation, particularly if the normal full pool is eventually raised 2 feet to elevation 1076 feet NGVD.

c. Moosehead Lake. Moosehead Lake has a gross usable storage capacity of about 544,000 acre-feet between elevations 1021.3 and normal full pool elevation 1029.0 feet NGVD, with discharge limitations from the lower foot of storage. With a surface area of 74,000 acres and a total drainage area of 1,268 square miles, a foot of surcharge storage represents 74,000 acre-feet of storage equivalent to 1.1 inches of runoff from its total watershed, or 2.5 inches of storage from the 558 square miles of net drainage area below Brassua. Therefore, it is concluded that a small increment of depth in Moosehead represents considerable flood control storage potential.

Moosehead has two regulating outlet locations: East and West; however, most flood regulation is done at the East Outlet. This facility is equipped with two 20-foot wide tainter gates, two 18-foot wide gated log sluices, and 17 other vertical gates, of varying types and widths, making up a total gated overflow width of about 320 feet with all gate sills at about elevation 1018.5 feet NGVD.

Historically, project operation has maintained surcharge storage levels to not over 1029.4 feet NGVD, or about 0.4 foot above normal full pool. The top of dam elevation at Moosehead is 1032.5 feet NGVD providing a minimum of only about 3 feet of freeboard above maximum historic lake levels.

It was concluded that project restraints severely limit using any significant depth of surcharge at this project, however, the appreciable amount of storage per unit depth emphasizes the importance of project gate operation and available storage utilization for overall effective operation during flood periods.

d. Flagstaff Lake. Flagstaff Lake has a usable storage capacity of about 276,000 acre-feet between elevation 1111 feet NGVD and normal full pool elevation 1146 feet NGVD. With a full pool surface area of 17,930 acres and a watershed area of 516 square miles, a foot of surcharge storage represents nearly 18,000 acre-feet of storage equivalent to about 0.65 inch of runoff. Reportedly, maximum surcharge storage utilized at the project during a flood period has been about 0.9 foot.

Flagstaff flows are regulated by two 7-foot low level sluices (invert elevation 1110) and five 20-foot wide tainter gates, sill elevation 1134.0 feet NGVD. The project has a 450-foot long spillway, crest elevation 1144 feet NGVD, equipped with 2 feet of flashboards resulting in a normal full pool level of 1146 feet NGVD. It was concluded that when pool levels exceed normal full pool the project quite rapidly becomes self-regulating and no appreciable surcharge storage could be utilized for added flood regulation without major modifications to the project's spillway.

The top of the earth embankment and the concrete nonoverflow section at Flagstaff are at elevations 1156 and 1153 feet NGVD, respectively.

6. MARCH/APRIL 1987 FLOOD

The most recent Kennebec flood was the result of high volume rainfall occurring on the last day of March and first day of April. The rainfall was produced by waves of low pressure moving northeasterly along a cold front creeping across New England from the west. The cold front and rainfall followed several days of daytime temperatures in the sixties. The high volume rainfall occurring under above average ripe snowpack conditions resulted in record runoff over much of the Kennebec Basin. Rainfall totals varied considerably over the basin with maximum amounts recorded in the central part of the basin in the region of Wyman Dam (Bingham). Maximums of 6 to 7 inches were experienced at the storm center with more nearly 3 inches in the regions of the upper headwater reservoirs and 4 to 5 inches in the lower basin. The resulting runoff produced new floods of record in the Kennebec Basin generally from the mouth of the Carrabassett tributary downstream throughout the middle and lower basin. Peak flows on the lower main stem Kennebec and tributaries: Sandy, Carrabassett and Sebasticook Rivers ranged from 20 to 30 percent greater than the earlier greatest flood of March 1936. Though coincident snowpack conditions during the recent rainfall produced appreciable snowmelt runoff, it was fortunate that ice had generally gone out of the rivers prior to the event, (a factor contributing to damages in 1936) and that the three upstream storage reservoirs were in a prespring runoff, drawn down state. Therefore, they completely controlled runoff from their contributing watersheds.

Computed inflows, outflows, and changes in storage at Moosehead and Flagstaff Reservoirs are shown graphically on plates 10 and 11. This event dramatically demonstrated, as was stated in the earlier 1985 report, that there is potential for major flooding on the Kennebec from watershed runoff

downstream of the three large upper basin storage reservoirs. On the other hand, had the recent event occurred under conditions of near full reservoirs, such as in June 1984, it is estimated that flows in the lower Kennebec, in the vicinity of the North Sidney gage, could have been in the order of 20 percent greater, with resulting flood stages in the order of 4 feet higher. Fortunately, having full snowpack conditions under full reservoir conditions would be quite unlikely.

Because of the reservoirs the upper basin above Bingham, representing 50 percent of the watershed above Augusta, contributed only about 25 percent of the peak flow at Augusta. By comparison the intervening 1513 square miles of watershed between Bingham and Waterville, including the Sandy and Carrabassett tributaries, representing only about 30 percent of the watershed at Augusta, contributed about 60 percent of the peak floodflow at Augusta.

Flood hydrographs and component contributions to peak flows, estimated and recorded, are shown graphically on plates 10 through 12. It is noted that much of the 1987 flood analysis was based on provisional postflood USGS data subject to revision prior to publication. Also an indepth, more authoritative hydrologic report, is being prepared by the Maine U.S. Geological Survey and will be available for future reference.

In analyzing the 1987 flood, the local contribution hydrograph between the Forks and Bingham gages was computed by lagging the Forks hydrograph 1 hour and subtracting from the Bingham data. Component contributions at North Sidney were computed by lag/averaging the Bingham hydrograph 16/7 hours and lagging the Carrabassett and Sandy River hydrographs 12 hours.

7. SUMMARY

All season reservoir regulation guide curves were developed by trial through multiyear sequential hydrologic system simulations. The objective was to maximize reservoir storage availability for incidental flood control while not adversely impacting hydropower capability. Simulations, using the developed guide curves, indicated that they would result in little change in downstream flow regime but provide significantly greater reservoir storage availability. Storage capacity of 570,000 acre-feet, equivalent to 6 inches of flood runoff, would be available about 65 percent of the time as compared with less than 40 percent under actual operations. Guide curve operation would likely minimize spillage during nonspring refill floods such as the December 1973 event, but would not eliminate all spillage during critical spring refill season floods such as April 1983 and June 1984. Because

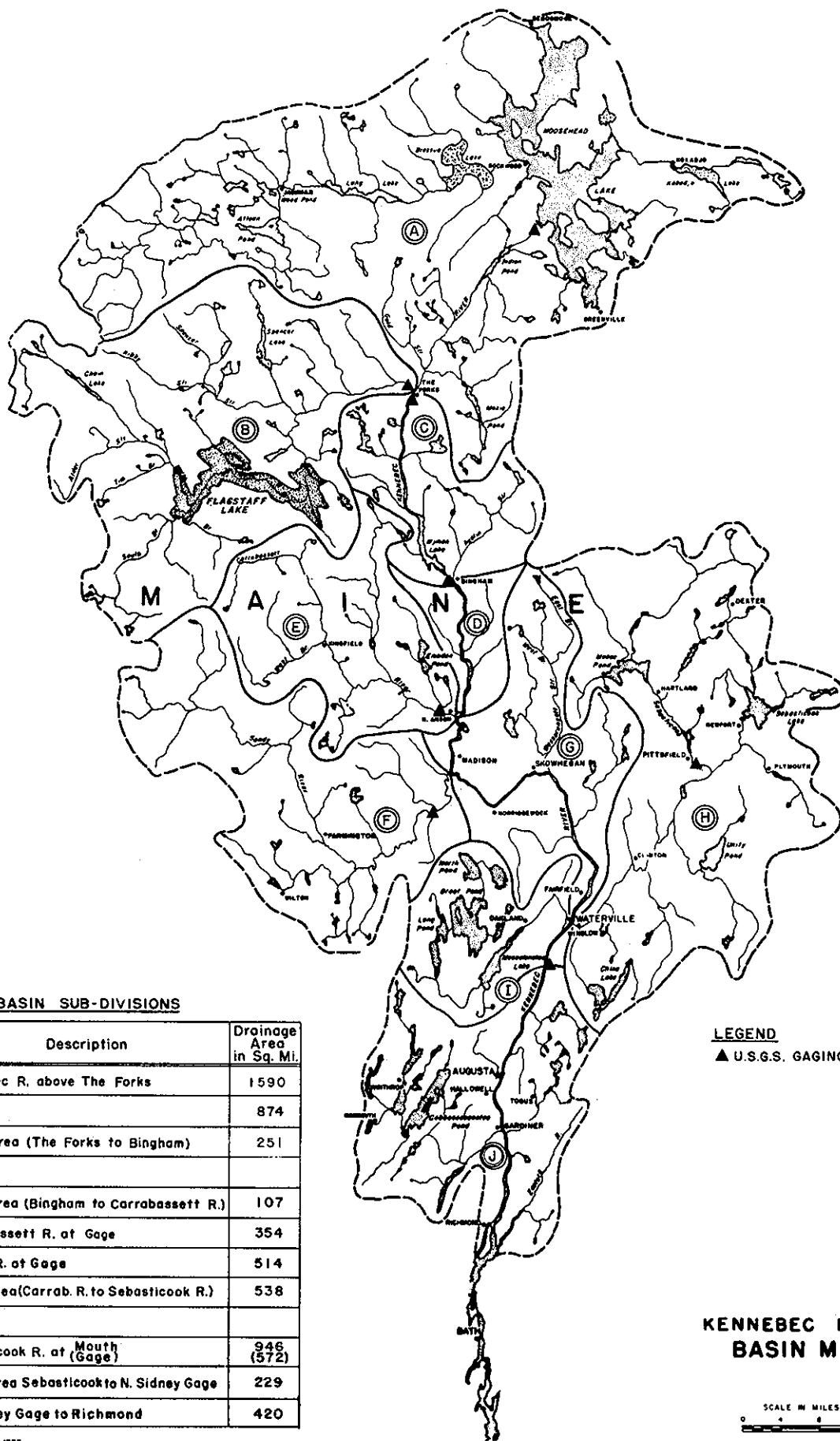
spring refill is the most critical flood season, spring season (April and May) guide curves were explored that might aid orderly spring refill, minimize potential for premature spring refill, while not impacting storage capability during drought years.

In applying the guide curves to past flood events it was found impossible in most instances to prevent spillage. Average April to May runoff in the upper Kennebec is about 11 inches, or equivalent to total usable reservoir storage; therefore, when abnormal spring runoff, as high as 17 inches, occurs then spillage is inevitable. Therefore, secondary guidance was added to the guide curves in an effort to modify peak rates of spillage when spillage was eminent. Applying the guidance to the experienced April 1979, April 1983 and June 1984 flood events indicated potential reductions of about 30 percent in peak rates of spillage.

Cursory analyses were made of the relative effectiveness of flood control storage in various presently uncontrolled subwatersheds upstream of Waterville, Maine. Resulting average main stem flood stage reduction per 100,000 acre-feet of storage varied from about 1.0 to 2.5 feet for different subwatersheds with maximum effectiveness indicated for the Carabassett tributary.

A review of surcharge storage characteristics at the three storage reservoirs: Brassua, Moosehead and Flagstaff, revealed no opportunity for any significant added use of surcharge storage for flood control. An amount of surcharge storage is required for gate operation and for the establishment of gate operation schedules, which result in some incidental modification between peak inflow and outflow. The large amount of surcharge storage, per unit depth at these large lake areas, emphasizes the importance of gate operating schedules and available storage utilization for effective project operation during floods.

The most recent major Kennebec River flood of March/April 1987 was analyzed, and component contributions determined, using provisional streamflow and rainfall records. This was a new flood of record generally throughout the mid to lower Kennebec Basin and, with the upper basin reservoirs completely controlling the runoff from their contributing watersheds, dramatically demonstrated the flood producing potential of runoff from the uncontrolled downstream watersheds.



BASIN SUB-DIVISIONS

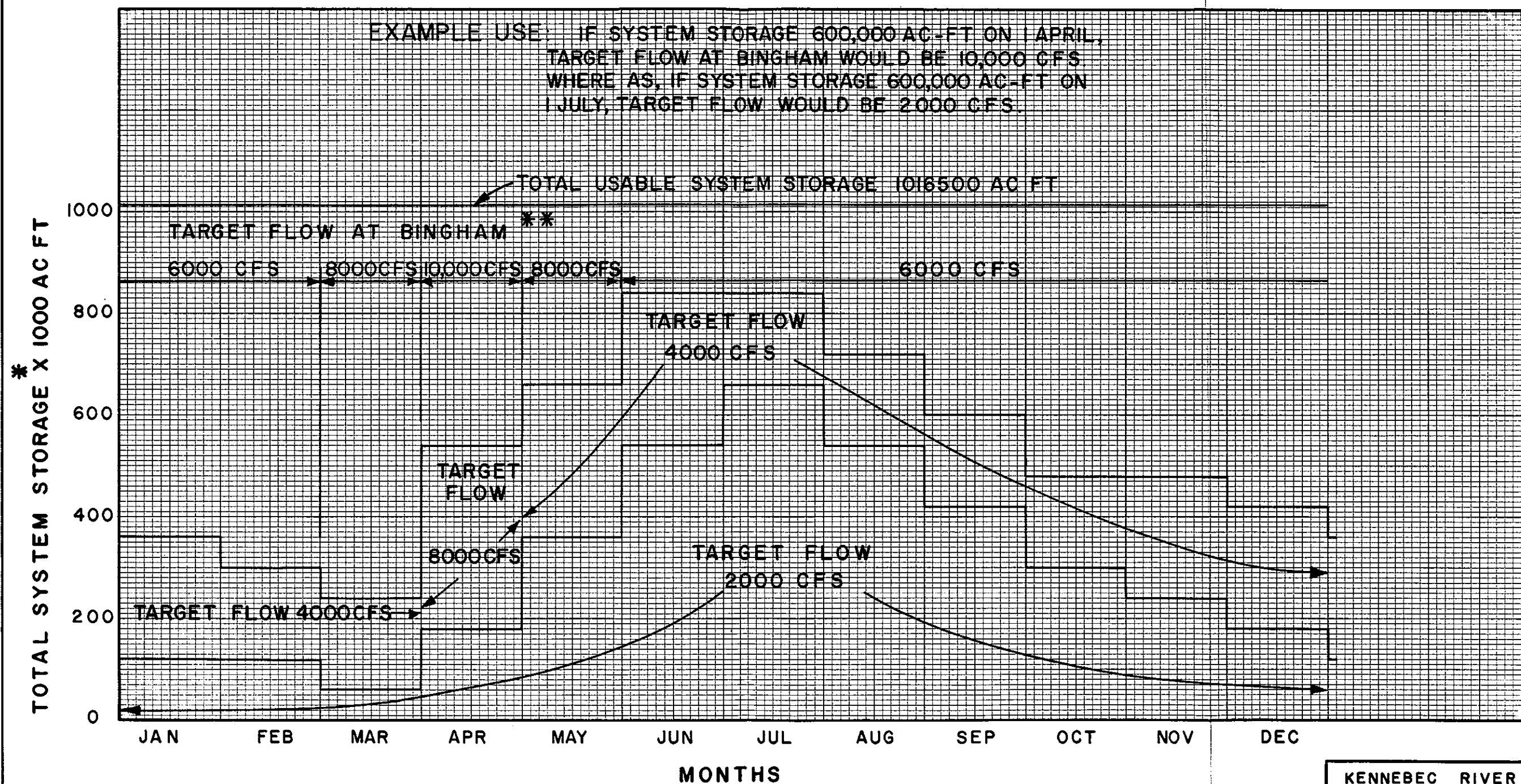
Area	Description	Drainage Area in Sq. Mi.
(A)	Kennebec R. above The Forks	1590
(B)	Dead R.	874
(C)	Local area (The Forks to Bingham)	251
(D)	Local area (Bingham to Carrabassett R.)	107
(E)	Carrabassett R. at Gage	354
(F)	Sandy R. at Gage	514
(G)	Local area (Carrab. R. to Sebasticook R.)	538
(H)	Sebasticook R. at Mouth (Gage)	946 (572)
(I)	Local area Sebasticook to N. Sidney Gage	229
(J)	N. Sidney Gage to Richmond	420

LEGEND

▲ U.S.G.S. GAGING STATIONS

KENNEBEC RIVER BASIN MAP

SCALE IN MILES
0 4 8 12



* SYSTEM STORAGE REFERS TO THE THREE LAKES
BRASSUA, MOOSEHEAD AND FLAGSTAFF

** TARGET FLOWS ARE ON KENNEBEC RIVER
AT BINGHAM

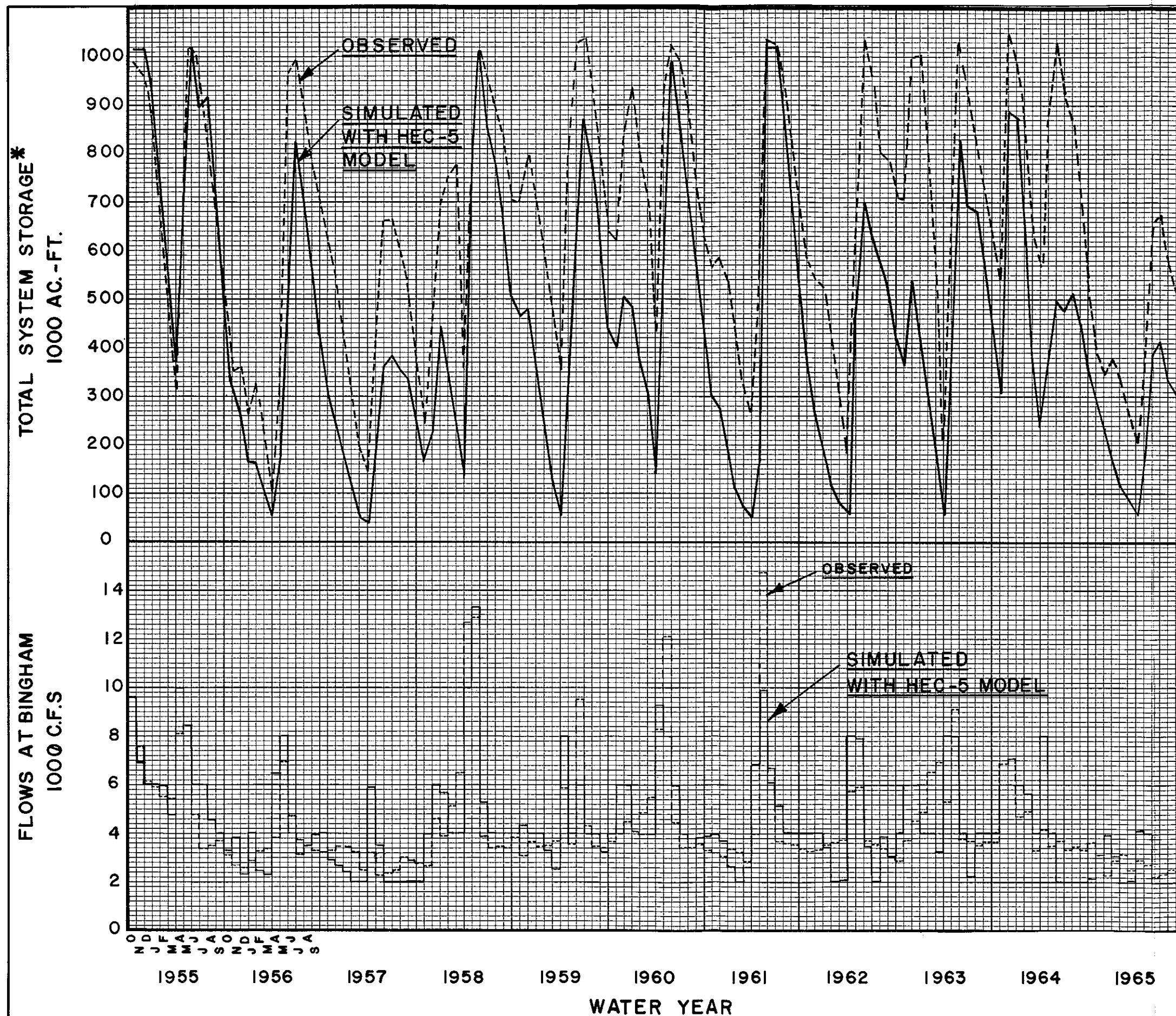
KENNEBEC RIVER BASIN
MONTHLY GUIDE
CURVES

FOR LAKE REGULATION

HES

JULY 1987

PLATE 2



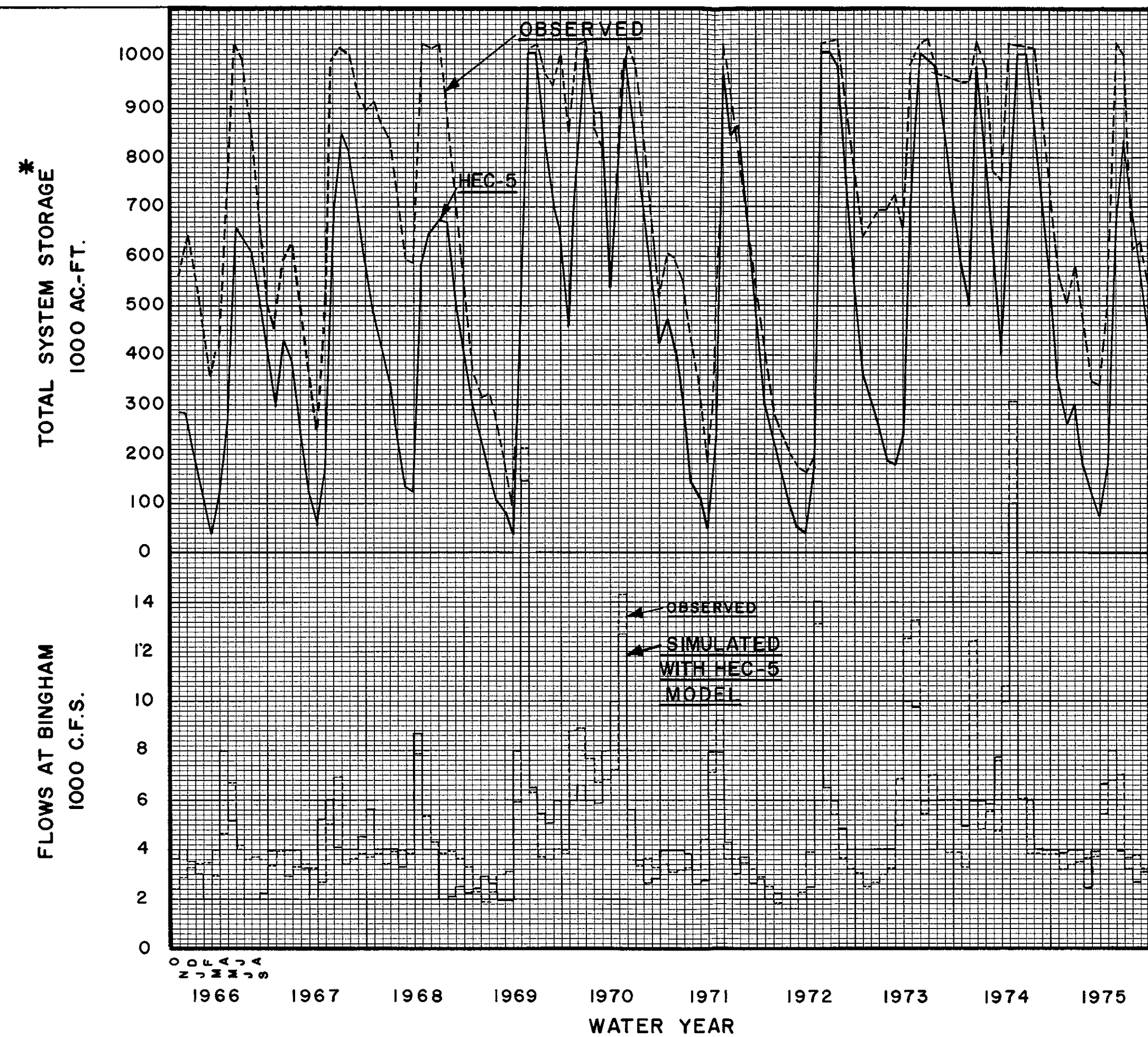
* SYSTEM STORAGE REFERS TO THE THREE LAKES: BRASSUA, MOOSEHEAD & FLAGSTAFF.

KENNEBEC RIVER BASIN
 TOTAL SYSTEM STORAGE
 AND FLOWS AT BINGHAM
 OBSERVED & SIMULATED

HES

JULY 1987

PLATE 3



* SYSTEM STORAGE REFERS TO THE THREE LAKES: BRASSUA, MOOSEHEAD & FLAGSTAFF.

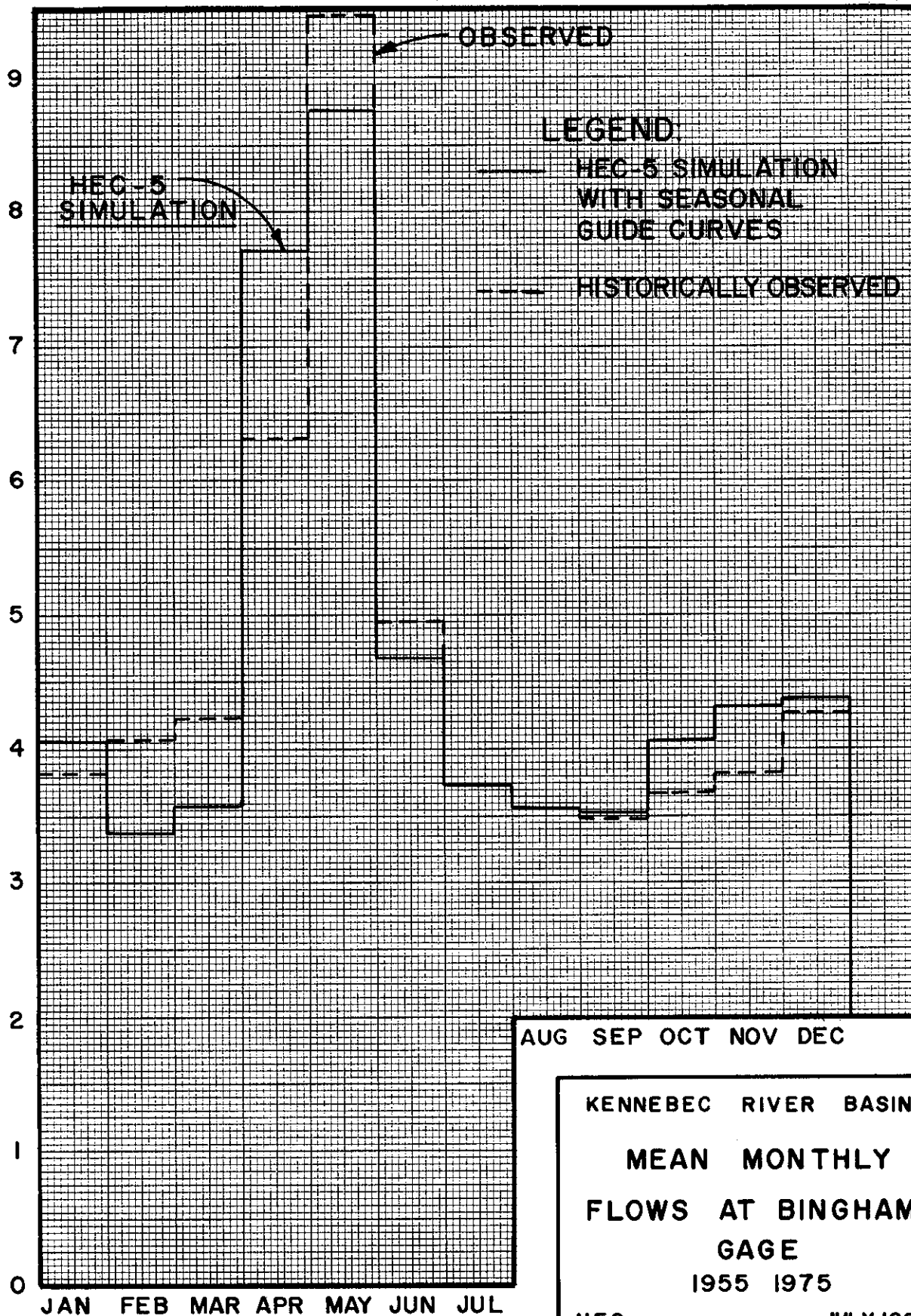
KENNEBEC RIVER BASIN
 TOTAL SYSTEM STORAGE
 AND FLOWS AT BINGHAM
 OBSERVED & SIMULATED

HES

JULY 1987

PLATE 4

MEAN MONTHLY DISCHARGE AT BINGHAM 1000 CFS



KENNEBEC RIVER BASIN

MEAN MONTHLY
FLOWS AT BINGHAM
GAGE

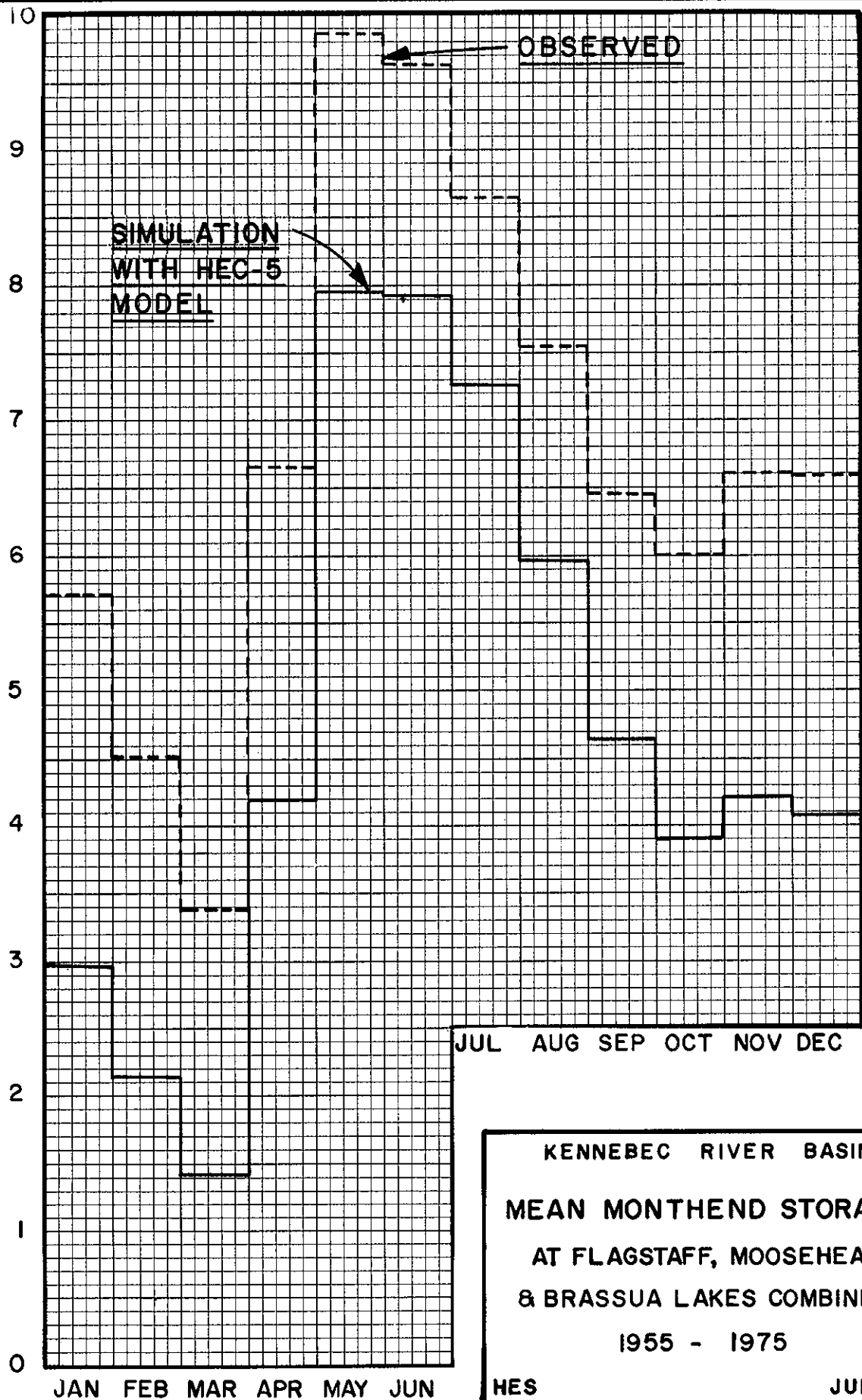
1955 1975

HES

JULY 1987

PLATE 5

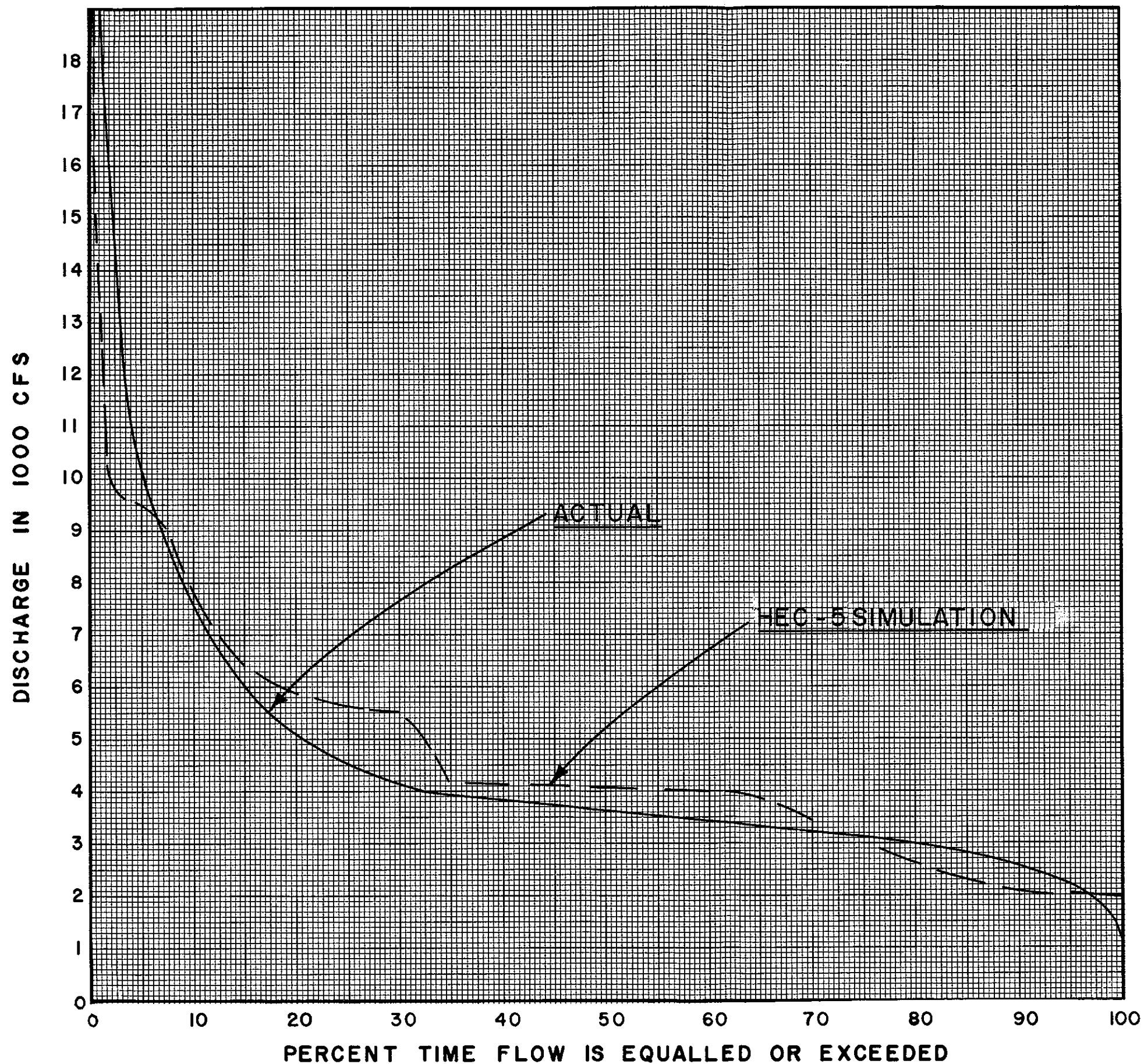
MEAN MONTHEND STORAGE AT FLAGSTAFF, MOOSEHEAD, & BRASSUA LAKE IN AC - FT x 1000000



KENNEBEC RIVER BASIN
MEAN MONTHEND STORAGE
AT FLAGSTAFF, MOOSEHEAD,
& BRASSUA LAKES COMBINED
1955 - 1975

HES

JULY 87



NOTES:

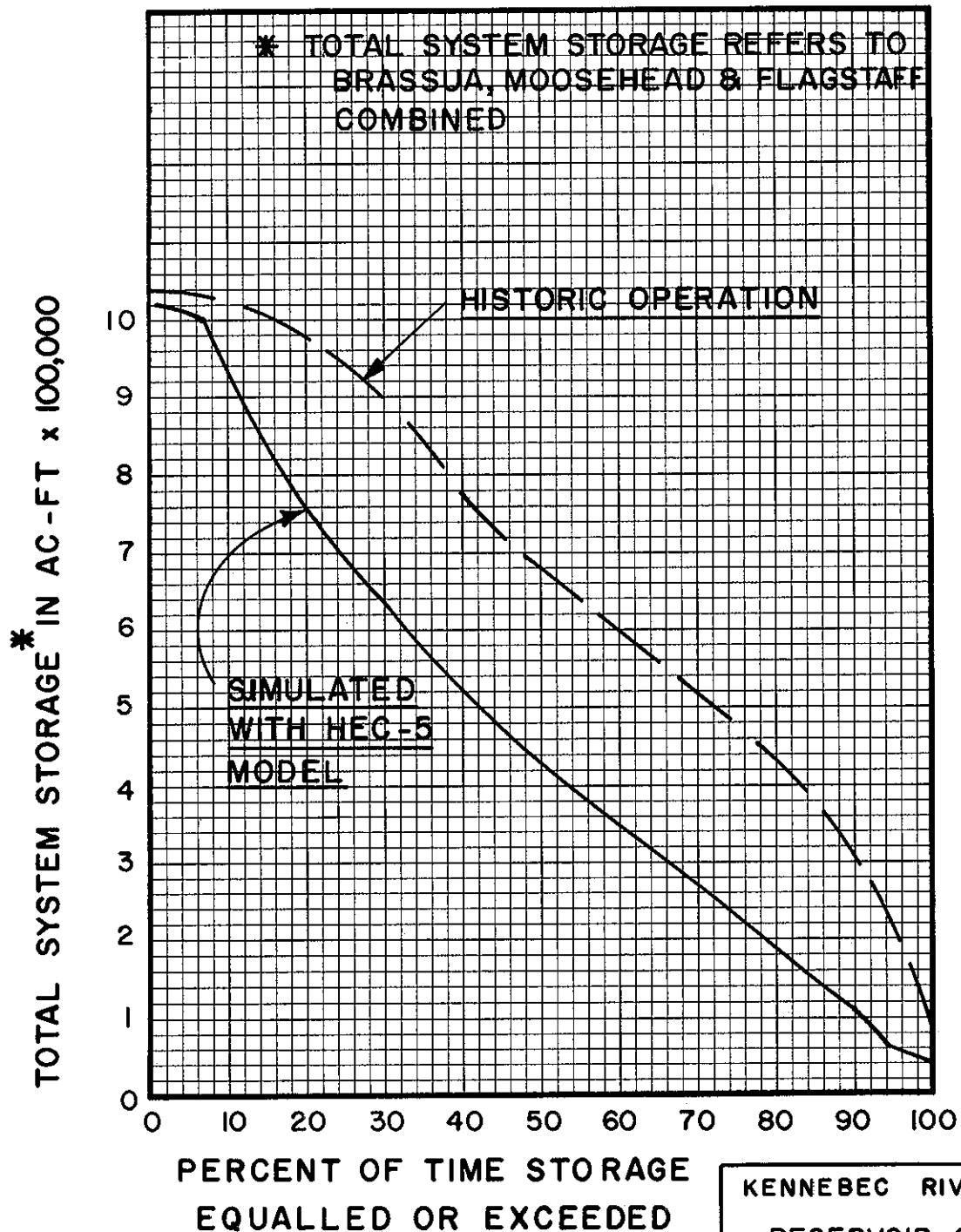
D.A. = 2715 SQ. MI.
PERIOD OF ANALYSIS
1955 - 1975

KENNEBEC RIVER BASIN
FLOW DURATION
CURVES AT
BINGHAM

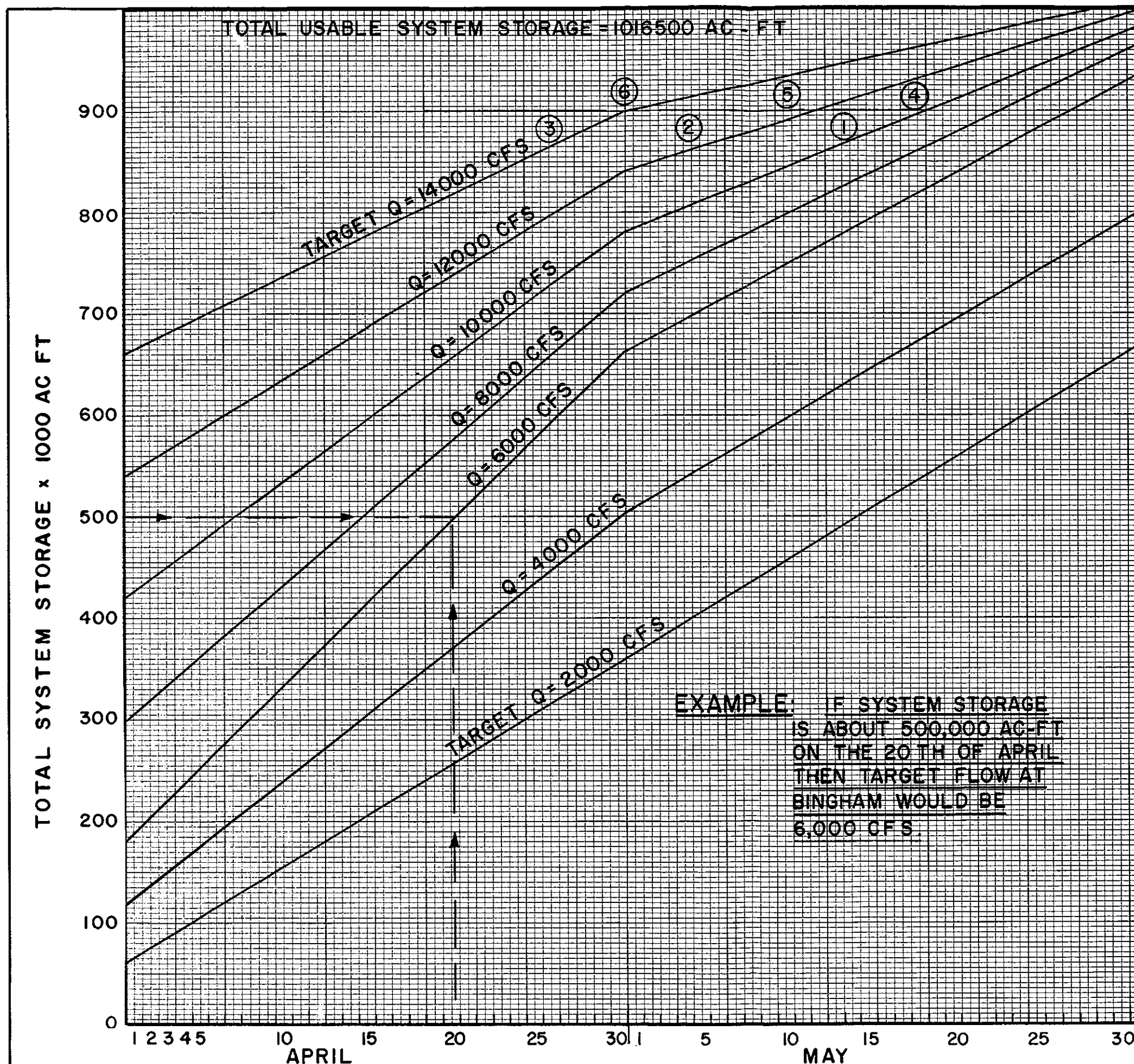
HES

JULY 1987

PLATE 7



KENNEBEC RIVER BASIN
RESERVOIR SYSTEM
STORAGE - DURATION
CURVES
1955 - 75 TEST PERIOD



NOTES:

STOR. < 900,000

- ① TARGET "Q" < 12,000
NO MIN. RELEASE RATE
- ② TARGET "Q" 12-14 K
MIN. RELEASE = > 8 K
- ③ TARGET "Q" > 14,000
MIN. RELEASE = > 10 K

STOR. > 900,000

- ④ TARGET "Q" < 12,000
MIN. RELEASE = > 1/2 IN FLOW
- ⑤ TARGET "Q" 12-14 K
MIN. RELEASE = > 1/2 IN FLOW
OR 8 K
- ⑥ TARGET "Q" > 14 K
MIN. RELEASE = > 1/2 IN FLOW
OR 10 K

LEGEND

- < LESS THAN
- > GREATER THAN
- => NOT LESS THAN

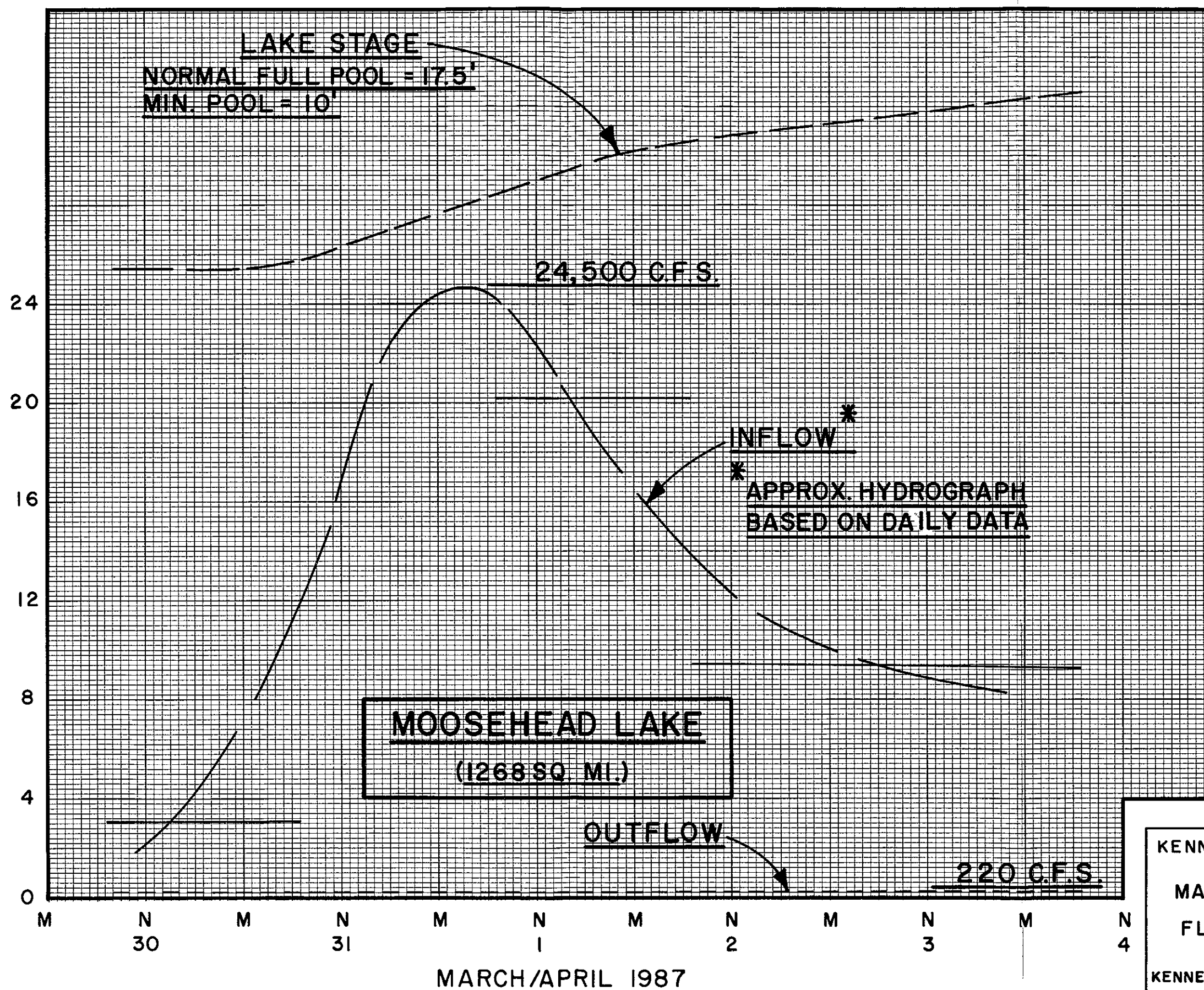
KENNEBEC RIVER BASIN
RESERVOIR STORAGE
SPRING REFILL
GUIDE CURVES

HES

JULY 1987

PLATE 9

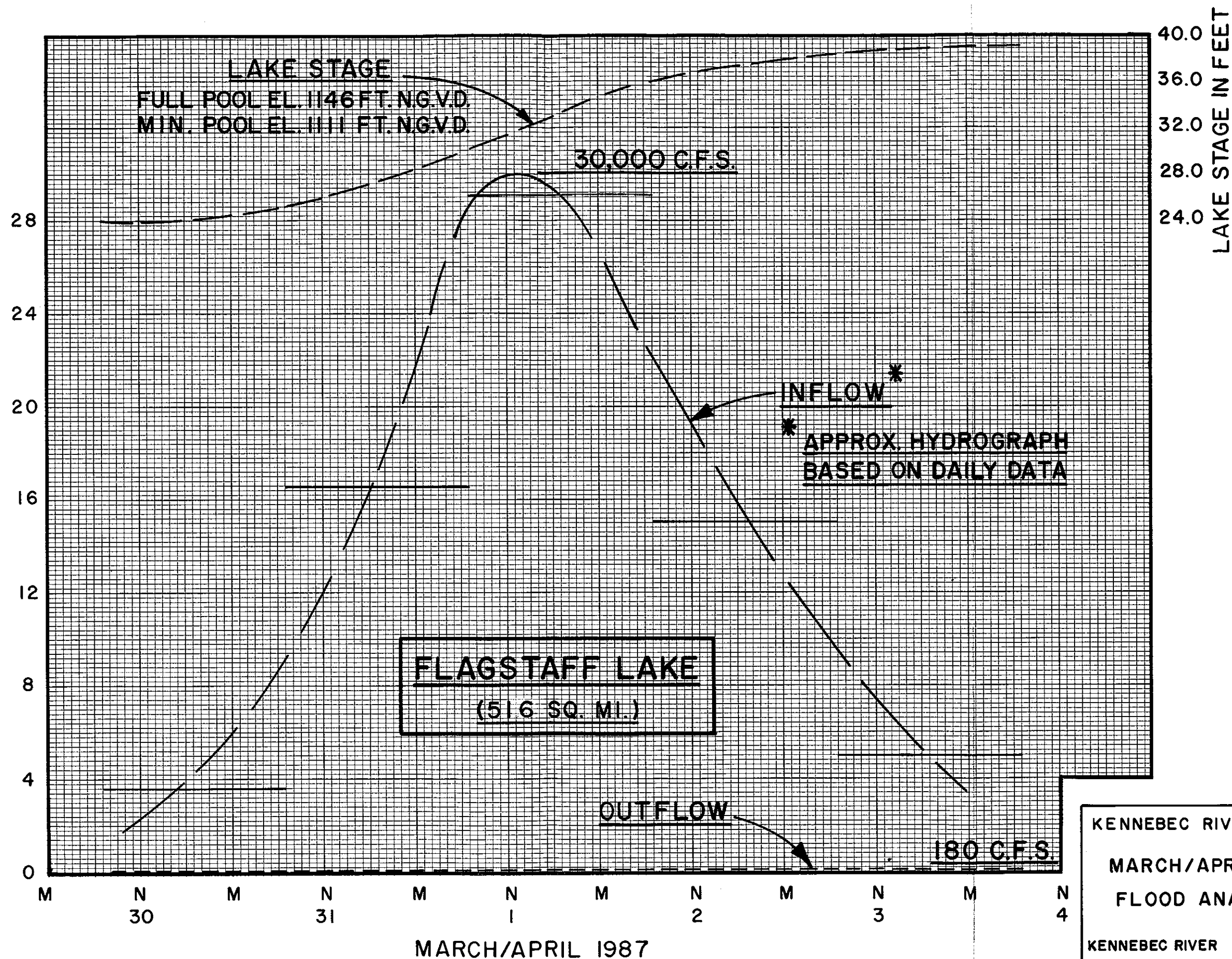
DISCHARGE IN 1000 C.F.S.



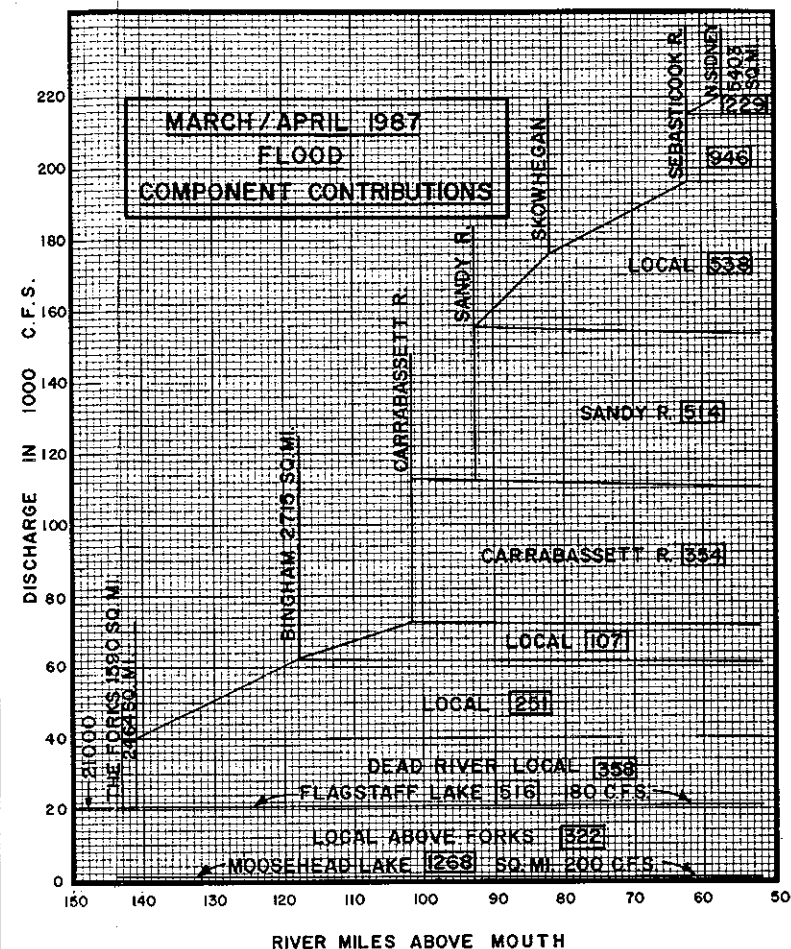
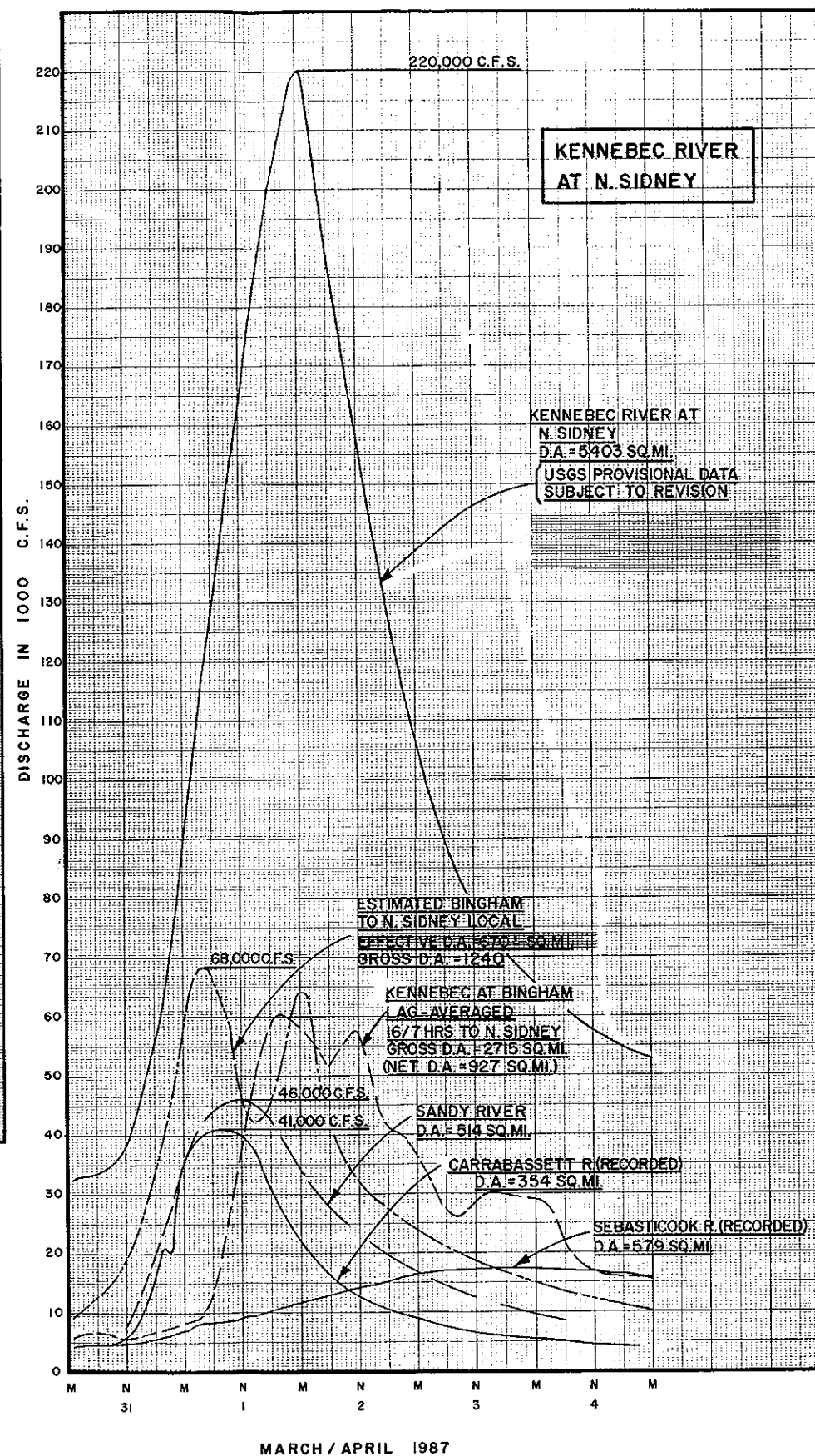
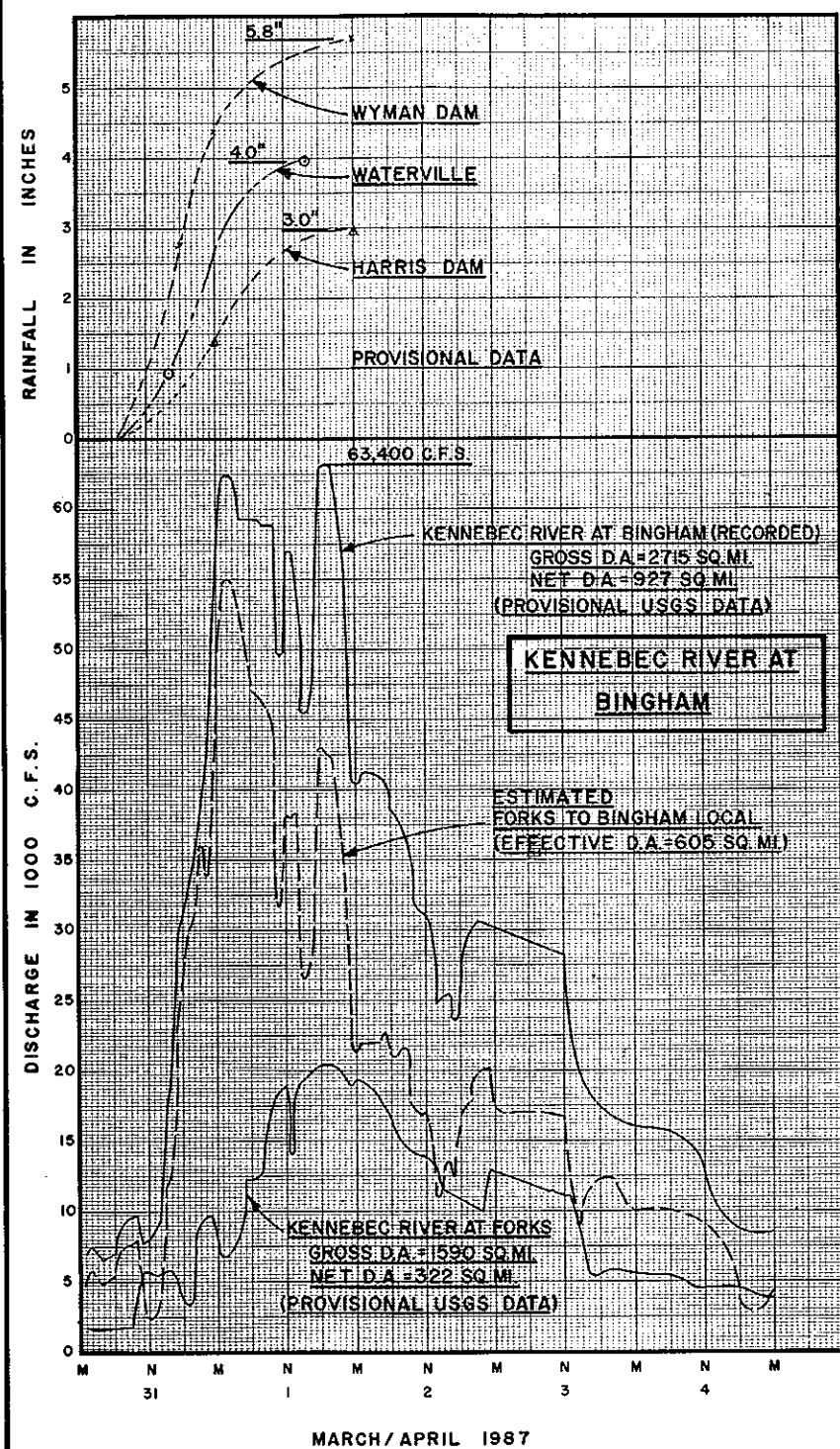
LAKE STAGE IN FEET

KENNEBEC RIVER BASIN
MARCH/APRIL 1987
FLOOD ANALYSIS
KENNEBEC RIVER MAINE

DISCHARGE IN 1000 C.F.S.



KENNEBEC RIVER BASIN
MARCH/APRIL 1987
FLOOD ANALYSIS
KENNEBEC RIVER MAINE



DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION
CORPS OF ENGINEERS
WALTHAM, MASS.

KENNEBEC RIVER BASIN

FLOOD ANALYSIS

MARCH - APRIL 1987

A P P E N D I X

HEC-5 COMPUTER
INPUT-OUTPUT

BRASSUA, MOOSEHEAD &
FLAGSTAFF SYSTEM SIMULATION
USING SEASONAL GUIDE CURVES

SEPTEMBER 1987

5 SIMULATION OF FLOOD CONTROL
AND CONSERVATION SYSTEMS

APRIL 1982 VERSION (UPDATED 14 FEB 83)

MAX DIMENSION LIMITS ARE CURRENTLY SET AT 35 RESERVOIRS AND 55 CONTROL POINTS

*INPUT LISTING FROM HEC5A

TO SUPPRESS LISTING, INSERT NCLIST CARD INTO INPUT DECK AT DESIRED POINT

T1 KENNEBEC RIVER BASIN STUDY

T2 BRASSUA MOOSEHEAD & FLAGSTAFF OPERATING

T3 FOR FRM YIELD AT BINGHAM

J1	0	10	6	5	6	2	0	10		
J2				16						
J3	4									
JZ	1.09	1.11	1.10	2.09	2.11	2.10	3.11	3.10	4.24	4.04
RL	1	196500	0	47800	123500	160000	196500	196500		
RL	1	1	0	0	0	0	0	0	0	0
RL					0	0	0	0	0	0
RL	2	1	0	0	45000	35000	15000	7000	7000	7000
RL					15000	60000	110000	140000	110000	80000
RL	3	1	0	0	57000	49000	34000	22000	20000	15000
RL					42000	88000	133000	147000	117000	87000
RL	4	1	0	0	76000	72000	57000	41000	35000	225000
RL					76000	114000	159000	166000	136000	106000
RL	5	1	0	0	95000	95000	80000	60000	50000	30000
RL					110000	140000	185000	185000	155000	125000
RL	6	1	0	0	196500	196500	196500	196500	196500	196500
RL					196500	196500	196500	196500	196500	196500
RO	1	2								
RS	4	0	7270	120800	196500					
RQ	4	8000	8000	8000	8000					
RE	4	1030	1040	1050	1073					
CP	1	2000	142	142						
ID BRASSUA										
C1	1	.26								
RT	1	2								
RL	2	544000	0	70800	206000	408800	544000	544000		
RL	1	2	0	0	0	0	0	0	0	0
RL					0	0	0	0	0	0
RL	2	2	0		170000	135000	110000	75000	75000	35000
RL					110000	200000	285000	345000	285000	225000
RL	3	2	0	0	187000	173000	143000	118000	99000	67000
RL					163000	251000	341000	367000	307000	247000
RL	4	2	0	0	221000	214000	184000	159000	132000	101000
RL					224000	298000	388000	401000	341000	281000
RL	5	2	0	0	255000	255000	225000	200000	165000	135000
RL					285000	345000	435000	435000	375000	315000
RL	6	2	0	0	544000	544000	544000	544000	544000	544000
RL					544000	544000	544000	544000	544000	544000
RO	1	4								
RS	4	0	70800	408800	544000					
RQ	4	20000	20000	20000	20000					

RL	1	1000	1010	1020	1029						
CP	2	8000	250	250							
IDMOOSEHEAD											
C1	2	.21									
RT	2	4									
RL	3	276000	3	82100	137500	220600	276000	276000			
RL	1	3	0	0	0	0	0	0	0	0	0
RL					0	0	0	0	0	0	0
RL	2	3	3	0	85000	70000	55000	38000	38000	18000	
RL					55000	100000	145000	175000	145000	115000	
RL	3	3	0	0	102000	92000	77000	62000	53000	37000	
RL					85000	125000	170000	192000	162000	132000	
RL	4	3	3	0	116000	110000	96000	81000	69000	56000	
RL					117000	150000	195000	206000	176000	146000	
RL	5	3	0	0	130000	130000	115000	100000	85000	75000	
RL					145000	175000	220000	220000	190000	160000	
RL	6	3	0	0	276000	276000	276000	276000	276000	276000	
RL					276000	276000	276000	276000	276000	276000	
RO	1	4									
RS	4	0	82100	220600	276000						
RO	4	5000	5000	5000	5000						
RE	4	1080	1100	1120	1144						
CP	3	8000	104	104							
IDFLAGSTAFF											
C1	3	.19									
RT	3	4									
CP	4	8000	4000	2000							
IDBINGHAM GAGE											
C1	4	.34									
RT	4										
CC	12	6000	6000	6000	6000	6000	8000	10000	8000	6000	
CC	6000	6000	6000								
QM	4000	4000	4000	4000	4000	4000	8000	4000	4000	4000	
QM	4000	4000									
ED											
SF	0	412	0	051060100	0	720					
ZW A=KENNEBEC F=BASE											

IN	1 JUNE 1951	2123	2880	1331	2208	1477	7849	4452	2366
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IN	1931	5139	6424	1801	2102	3382	17070	13520	8536
IN	4889	9770	9598	6947	4745	2295	2426	2365	16370
IN	3999	6254	1711	180	196	2614	903	3935	1581
IN	8568	17170	5227	1887	1010	1806	2020	1891	1680
IN	868	1846	8286	6449	2389	1571	1630	626	576
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IN	1560	2210	16700	7260	2610	825	1030	970	875
IN	2260	3090	6550	9860	21200	10700	4100	1960	1120
IN	1150	10900	9590	2980	2870	5100	22100	13500	11600
IN	940	500	690	1530	1830	1510	3190	5449	9660
IN	2510	1750	720	1850					4600

*USERS

USER DESIGNED OUTPUT

LOC NO=					SUMMARY BY PERIOD FLOOD= 1									
CODE=					1.	1.	1.	2.	2.	2.	3.	3.	4.	4.
					1.090	1.110	1.100	2.090	2.110	2.100	3.110	3.100	4.240	4.140
PER	DY	MO	YR	DW	BRASSUA INFLOW	BRASSUA EOP STOR	BRASSUA OUTFLOW	MOOSEHEAD INFLOW	MOOSEHEAD EOP STOR	MOOSEHEAD OUTFLOW	FLAGGSTAF ECP STOR	FLAGGSTAF OUTFLOW	SINGHAM 6 LOCAL IN	SINGHAM 6 FLOW REG
1	1	6	51	1	551.20	185000.00	744.46	1189.66	435000.00	3021.44	220000.00	1343.90	720.80	5086.14
2	1	7	51	1	748.80	185000.11	748.80	1353.60	386219.04	2146.93	199513.72	873.87	979.20	4000.10
3	1	8	51	1	346.06	137512.72	1118.36	1397.87	307359.38	2680.38	162147.98	867.08	452.54	4000.30
4	1	9	51	1	574.08	94482.64	1297.21	1760.89	266057.34	2454.99	139247.14	794.29	750.72	4000.10
5	1	10	51	1	384.12	66514.52	838.87	1149.04	181868.55	2518.22	96668.55	979.60	502.18	4000.30
6	1	11	51	1	2040.74	95000.00	1562.03	3210.32	255000.00	1981.33	130000.00	934.53	2668.66	5584.51
7	1	12	51	1	1157.52	80001.16	1401.45	2336.37	225000.00	2824.27	115000.00	1089.83	1513.68	5427.77
8	1	1	52	1	615.16	60001.73	940.41	1437.27	172343.60	2293.64	87183.62	901.92	804.44	4000.00
9	1	2	52	1	549.64	43086.48	843.71	1287.65	109746.50	2375.89	58210.42	905.35	718.76	4000.30
10	1	3	52	1	301.60	52900.05	142.00	385.60	35000.00	1601.22	18000.00	874.35	394.40	2869.97
11	1	4	52	1	3641.30	150565.60	2000.00	4941.05	204577.30	2091.25	108084.66	1147.05	4761.70	8000.30
12	1	5	52	1	2983.66	196500.00	2136.62	4465.73	345000.00	2182.01	175000.00	1019.03	3770.94	6971.98
13	1	6	52	1	1591.98	187543.17	1742.50	3028.33	435000.00	1515.85	220000.00	407.13	2081.82	4004.81
14	1	7	52	1	39.52	181241.83	142.00	173.92	345000.00	1637.61	175000.00	760.72	51.68	2450.31
15	1	8	52	1	29.64	121388.77	1003.04	1026.98	285000.00	2002.77	145000.00	509.56	38.76	2551.09
16	1	9	52	1	58.76	82749.08	708.11	755.57	225000.00	1763.89	115000.00	547.10	76.84	2387.83
17	1	10	52	1	226.20	46137.67	821.62	1004.32	170000.00	1898.80	85000.00	653.20	295.80	2847.79
18	1	11	52	1	268.84	34143.99	470.40	687.54	135000.00	1275.72	70000.00	448.54	351.56	2075.82
19	1	12	52	1	777.92	14924.62	1090.49	1718.81	110000.00	2125.39	55000.00	812.43	1017.28	3955.10
20	1	1	53	1	651.04	6991.10	780.06	1305.90	75000.00	1875.12	38000.00	752.23	851.36	3478.71
21	1	2	53	1	634.92	0.00	760.88	1273.62	75000.00	1273.62	38000.00	463.98	830.28	2567.88
22	1	3	53	1	2771.60	47444.53	2000.00	4238.69	147817.87	3054.35	81299.25	1321.22	3624.40	7999.96
23	1	4	53	1	5210.40	196500.00	2705.48	6913.88	449362.66	1846.32	228133.24	1340.01	6813.60	9999.93
24	1	5	53	1	2363.92	196500.00	2363.92	4273.24	494013.35	3547.08	250629.89	1361.61	3091.28	7999.97
25	1	6	53	1	514.28	194250.23	552.09	967.47	416444.07	2271.04	210129.83	1056.44	672.52	4000.30
26	1	7	53	1	326.04	182578.16	515.87	779.21	345000.00	1941.11	175000.00	809.58	426.36	3177.36
27	1	8	53	1	166.66	121867.83	1154.00	1288.61	285000.00	2264.41	145000.00	609.69	217.94	3092.03
28	1	9	53	1	180.70	82864.72	836.16	982.11	225000.00	1990.43	115000.00	636.21	236.30	2862.94
29	1	10	53	1	502.06	46185.52	1098.58	1504.09	170000.00	2398.57	85000.00	854.79	656.54	3909.39
30	1	11	53	1	1336.14	35572.46	1514.50	2593.69	220310.81	1748.20	113078.44	504.54	1747.26	4000.30
31	1	12	53	1	1670.24	80000.00	947.71	2296.75	225000.00	2220.48	115000.00	1189.31	2184.16	5593.95
32	1	1	54	1	468.26	60001.35	793.50	1171.71	148603.37	2414.17	76182.05	973.49	612.34	4000.30
33	1	2	54	1	546.52	37151.33	957.95	1399.37	92984.20	2400.83	49240.13	884.49	714.68	4000.00
34	1	3	54	1	879.32	63720.08	447.23	1157.45	50470.24	1848.86	27185.45	1001.26	1149.88	4000.00
35	1	4	54	1	4438.20	196500.00	2206.79	5791.49	285000.00	1850.15	145000.00	1263.39	5803.80	8917.34
36	1	5	54	1	3515.20	196500.00	3515.20	6354.40	510448.17	2687.89	258971.18	715.26	4596.80	7999.95
37	1	6	54	1	2219.36	196500.00	2219.36	4011.92	544000.00	3448.07	276000.00	1335.67	2902.24	7685.98
38	1	7	54	1	997.88	196498.04	997.91	1803.89	456182.09	3232.09	230682.54	1462.97	1304.92	5999.99
39	1	8	54	1	1271.14	166255.40	1762.98	2789.67	430666.99	3204.63	218327.58	1133.09	1662.26	5999.98
40	1	9	54	1	2540.20	196500.00	2031.93	4083.63	544000.00	2179.03	276000.00	887.10	3321.80	6387.93
41	1	10	54	1	2495.48	196500.00	2495.48	4511.06	544000.00	4511.06	276000.00	1823.62	3263.32	9598.30
42	1	11	54	1	1806.22	196498.04	1806.25	3265.12	544000.00	3265.12	276000.00	1319.93	2361.98	6947.33
43	1	12	54	1	1233.70	196500.00	1233.67	2230.12	492714.74	3064.18	250116.22	1322.50	1613.30	5999.98
44	1	1	55	1	596.70	180426.88	858.10	1340.05	352874.70	3614.30	178214.96	1605.39	780.30	5999.99
45	1	2	55	1	630.76	133328.59	1478.80	1988.26	181656.91	5071.15	203814.65	0.00	824.84	5895.99
46	1	3	55	1	614.90	162406.50	142.00	638.65	135000.00	1397.44	75000.00	2544.29	804.10	4745.33
47	1	4	55	1	4256.20	196500.00	3683.25	7120.95	367984.04	3205.58	186572.62	1228.57	5565.80	9999.94
48	1	5	55	1	3309.80	196500.00	3309.80	5983.10	544000.00	3120.52	276000.00	970.83	4328.20	8419.55
49	1	6	55	1	1039.74	196498.04	1039.77	1879.56	465343.80	3201.40	235689.47	1438.92	1359.66	5999.99
50	1	7	55	1	1626.04	182993.32	1748.09	3061.43	480619.72	2813.00	243437.65	1060.62	2126.36	5999.98
51	1	8	55	1	444.60	172087.06	719.55	1078.65	375000.00	2796.36	190000.00	1193.97	581.40	4571.73
52	1	9	55	1	46.80	130804.63	740.56	778.36	246984.95	2929.70	131988.37	1009.10	61.20	4000.00

LOC NO=

NO-	1.					2.					3.					4.					5.				
PER	DY	MO	YR	DW	BRASSUA INFLOW	BRASSUA EOP STOR	BRASSUA OUTFLOW	MOOSEHEAD INFLOW	MOOSEHEAD EOP STOR	MOOSEHEAD OUTFLOW	FLAGGSTAF ECP STOR	FLAGGSTAF OUTFLOW	BINGHAM 6 LOCAL IN	BINGHAM 3 FLOW REG											
53	1	10	55	1	50.96	72698.34	995.95	1037.11	170000.00	2289.14	85000.00	801.42	66.64	3157.20											
54	1	11	55	1	679.64	48371.75	1088.46	1637.40	135000.00	2225.58	70000.00	748.74	888.76	3863.38											
55	1	12	55	1	234.78	0.00	1021.46	1211.09	110000.00	1617.67	55000.00	415.52	307.02	2340.21											
56	1	1	56	1	1923.10	6160.07	922.92	1749.27	101854.58	1881.74	52588.60	780.36	1337.90	4000.00											
57	1	2	56	1	411.06	0.00	518.15	850.16	75000.00	1317.02	38000.00	560.96	537.54	2415.53											
58	1	3	56	1	332.54	0.00	332.54	601.13	35000.00	1251.66	18000.00	568.27	434.86	2254.79											
59	1	4	56	1	2227.68	15000.00	1975.60	3774.88	110000.00	2514.48	55000.00	1006.12	2913.12	6433.73											
60	1	5	56	1	4464.20	166519.96	2000.00	5605.70	345000.00	1783.85	232333.17	378.29	5837.80	7999.34											
61	1	6	56	1	1359.02	196500.00	855.20	1952.87	412391.54	820.33	207974.23	1402.49	1777.18	4000.00											
62	1	7	56	1	490.62	182108.95	724.66	1120.93	345000.00	2216.94	175000.00	894.80	641.58	3753.31											
63	1	8	56	1	262.60	121699.62	1245.05	1457.15	285000.00	2432.94	145000.00	679.80	343.40	3456.14											
64	1	9	56	1	469.56	82824.12	1122.87	1502.13	225000.00	2510.45	115000.00	847.30	614.04	3971.79											
65	1	10	56	1	525.20	46168.72	1121.33	1545.53	170000.00	2440.01	85000.00	871.70	686.80	3998.51											
66	1	11	56	1	491.66	35564.35	669.87	1066.98	135000.00	1655.17	70000.00	611.37	642.94	2909.48											
67	1	12	56	1	436.80	14678.67	776.47	1129.27	110000.00	1535.85	55000.00	563.15	571.20	2670.20											
68	1	1	57	1	352.82	0.00	591.54	876.51	75000.00	1445.72	38000.00	534.30	461.38	2441.41											
69	1	2	57	1	225.68	4647.42	142.00	324.28	30188.21	1131.15	15295.36	573.73	295.12	2000.00											
70	1	3	57	1	479.96	7000.00	441.70	829.36	22229.46	958.79	11432.29	413.57	627.64	2000.00											
71	1	4	57	1	2154.36	16185.19	2000.00	3740.06	110000.00	2265.05	55000.00	842.17	2817.24	5924.46											
72	1	5	57	1	1676.74	60415.10	957.42	2311.71	200000.00	848.02	100000.00	493.47	2192.66	3534.15											
73	1	6	57	1	621.14	88926.32	142.00	643.69	195282.15	722.98	99354.07	464.76	812.26	2000.00											
74	1	7	57	1	408.46	100733.52	216.44	546.35	170145.02	955.16	86305.44	510.70	534.14	2000.00											
75	1	8	57	1	423.80	61437.47	1062.88	1405.18	180939.05	1229.63	92056.71	216.17	554.20	2000.00											
76	1	9	57	1	162.76	40717.63	510.96	642.42	140264.82	1325.97	71690.91	461.19	212.84	2000.00											
77	1	10	57	1	149.76	0.00	811.96	932.92	110075.82	1423.89	55137.91	380.27	195.84	2000.00											
78	1	11	57	1	1317.94	17919.67	1016.79	2081.28	138676.44	1600.64	72128.47	675.90	1723.46	4000.00											
79	1	12	57	1	2460.64	80000.00	1451.01	3438.45	239436.56	1799.77	122286.16	982.44	3217.76	5999.37											
80	1	1	58	1	1170.52	64526.26	1422.17	2367.59	200000.00	3008.96	100000.00	1217.82	1530.68	5757.46											
81	1	2	58	1	514.28	51381.48	750.96	1166.34	131896.92	2392.58	68550.02	934.90	672.52	4000.00											
82	1	3	58	1	556.14	76846.33	142.00	591.19	39989.49	2085.90	20562.51	1186.84	727.26	4000.00											
83	1	4	58	1	5337.80	196500.00	3326.98	7638.28	376573.19	1981.89	191316.94	1037.84	6980.20	9999.33											
84	1	5	58	1	4563.00	196500.00	4563.00	8248.50	544000.00	5525.60	276000.00	1957.28	5967.00	13449.89											
85	1	6	58	1	656.50	196458.04	656.53	1186.78	435000.00	3018.56	220000.00	1420.85	858.50	5297.91											
86	1	7	58	1	727.48	186097.44	896.63	1484.21	390014.76	2215.81	201476.66	832.87	951.32	4000.00											
87	1	8	58	1	574.86	139266.83	1336.48	1800.79	349017.70	2467.53	179301.41	780.73	751.74	4000.00											
88	1	9	58	1	332.80	110045.59	823.87	1052.67	258819.78	2698.48	136866.97	956.32	435.20	4000.00											
89	1	10	58	1	867.88	83026.87	1356.08	2057.06	255000.00	2119.18	130000.00	745.90	1134.92	4000.00											
90	1	11	58	1	1145.56	95000.00	893.93	1819.19	255000.00	1819.19	130000.00	837.14	1498.04	4154.37											
91	1	12	58	1	527.54	80001.16	771.47	1197.56	183183.42	2365.53	95621.58	944.61	689.86	4000.00											
92	1	1	59	1	537.94	47586.24	1065.11	1499.60	126531.85	2420.94	65553.78	875.60	703.46	4000.00											
93	1	2	59	1	341.90	16898.32	894.46	1170.61	75000.00	2098.47	38000.00	753.18	447.10	3298.75											
94	1	3	59	1	345.28	0.00	620.10	898.98	35000.00	1549.51	18000.00	577.58	451.52	2578.61											
95	1	4	59	1	3668.60	99290.04	2000.00	4963.10	207746.25	2060.05	109539.26	1142.55	4797.40	8000.00											
96	1	5	59	1	1940.12	109448.58	1774.91	3341.93	345000.00	1109.74	175000.00	353.18	2537.08	4000.00											
97	1	6	59	1	2610.40	196500.00	1147.47	3255.87	447122.66	1539.67	226228.15	1046.69	3413.60	5999.37											
98	1	7	59	1	627.38	187254.56	777.74	1284.47	385426.59	2287.85	199587.42	891.73	820.42	4000.00											
99	1	8	59	1	362.18	138036.83	1162.62	1455.15	310492.94	2673.81	163438.27	852.57	473.62	4000.00											
100	1	9	59	1	76.70	95793.88	786.61	848.56	225000.00	2285.29	115000.00	870.07	160.30	3255.66											
101	1	10	59	1	881.92	51535.52	1601.70	2314.02	227993.63	2265.34	118879.73	581.38	1153.28	4000.00											
102	1	11	59	1	2033.46	95000.00	1303.03	2945.44	272784.50	2192.71	138584.56	1148.12	2659.14	5999.37											
103	1	12	59	1	1453.66	85306.91	1611.30	2785.41	262425.69	2953.88	133888.83	1145.16	1900.94	5999.38											
104	1	1	60	1	623.74	73395.17	817.46	1321.25	200000.00	2336.49	100000.00	1006.95	815.66	4159.11											

LOC	LOC	1.	1.	1.	2.	2.	2.	3.	3.	4.	
NO		BRASSUA	BRASSUA	BRASSUA	MOOSEHEAD	MOOSEHEAD	MOOSEHEAD	FLAGGSTAF	FLAGGSTAF	BINGHAM 6	BINGHAM 6
	PER DY MO YR DW	INFLOW	EOP STOR	OUTFLOW	INFLOW	EOP STOR	OUTFLOW	EOP STOR	OUTFLOW	LOCAL IN	FLOW REG
105	1 2 63 1	713.18	54085.53	1048.87	1624.90	162983.04	2268.44	84022.08	798.94	932.62	4000.00
106	1 3 60 1	387.40	41916.47	585.31	898.21	67537.60	2450.46	37300.43	1042.94	506.60	4000.00
107	1 4 60 1	4498.00	190559.96	2000.00	5633.00	285000.00	1978.48	145000.00	1477.08	5882.00	9337.55
108	1 5 60 1	3614.00	196500.00	3517.40	6436.40	522007.20	2581.90	264837.82	692.05	4726.00	7999.95
109	1 6 60 1	1923.88	195510.22	1040.51	1867.49	441696.09	2217.15	223440.19	1443.92	1338.92	5999.99
110	1 7 60 1	438.36	186542.21	582.58	936.64	351611.23	2401.71	180108.68	1025.05	573.24	4000.00
111	1 8 60 1	210.08	125654.82	1201.28	1370.96	285000.00	2454.27	145000.00	724.50	274.72	3453.49
112	1 9 60 1	438.62	83788.47	1142.87	1497.14	225000.00	2505.46	115000.00	824.69	573.58	3903.73
113	1 10 60 1	503.62	46567.76	1108.95	1515.72	170000.00	2410.19	85000.00	855.93	658.58	3924.70
114	1 11 60 1	914.68	35756.99	1096.36	1835.14	155348.60	2081.36	81780.77	722.52	1196.12	4000.00
115	1 12 63 1	620.62	22711.85	832.78	1334.05	110000.00	2071.56	55000.00	889.07	811.58	3772.21
116	1 1 61 1	377.52	0.00	746.89	1051.81	75000.00	1621.02	38000.00	552.35	493.68	2667.05
117	1 2 61 1	335.40	0.00	335.40	606.30	48828.33	1077.54	24739.69	483.86	438.60	2000.00
118	1 3 61 1	607.10	0.00	607.10	1097.45	35000.00	1322.34	18000.00	553.26	793.90	2669.50
119	1 4 61 1	2388.88	23140.30	2000.00	3929.48	110000.00	2669.08	55000.00	1123.92	3123.92	6916.93
120	1 5 61 1	6094.40	196500.00	3275.02	8197.42	544000.00	1139.19	276000.00	859.43	7969.60	9968.22
121	1 6 61 1	1601.60	196498.04	1601.63	2895.23	544000.00	2895.23	276000.00	1170.40	2094.40	6160.33
122	1 7 61 1	646.10	196500.00	646.07	1167.92	435000.00	2940.61	220000.00	1382.89	844.90	5168.40
123	1 8 61 1	269.62	158961.00	880.12	1097.89	336288.58	2703.26	174060.00	944.16	352.58	4000.00
124	1 9 61 1	457.86	112542.49	1237.94	1607.75	278545.90	2578.13	144989.49	823.13	598.74	4000.00
125	1 10 61 1	316.16	77465.84	886.62	1141.98	186214.03	2643.59	101214.03	942.97	413.44	4000.00
126	1 11 61 1	605.28	57540.55	940.13	1429.01	136811.96	2259.23	71049.03	949.25	791.52	4000.00
127	1 12 61 1	752.18	23898.22	1299.31	1906.84	115061.33	2260.58	58374.22	755.80	983.62	4000.00
128	1 1 62 1	569.66	8524.56	819.68	1279.79	75000.00	1931.32	38000.00	747.64	744.94	3423.90
129	1 2 62 1	339.82	0.00	493.31	767.78	55112.87	1125.86	27523.86	429.76	444.38	2000.00
130	1 3 62 1	440.70	7000.00	326.86	682.81	35000.00	1009.91	18000.00	483.44	576.30	2069.55
131	1 4 62 1	3900.00	120659.50	2000.00	5150.00	234606.80	1795.55	121868.70	1104.45	5100.00	8000.00
132	1 5 62 1	3016.00	182531.82	2000.00	4436.00	345000.00	2640.65	175000.00	1339.91	3944.00	7924.57
133	1 6 62 1	558.48	196500.00	323.74	774.82	285000.00	1783.14	145000.00	912.28	730.32	3425.74
134	1 7 62 1	301.60	148952.24	1074.88	1318.48	282566.55	1358.05	143330.86	247.55	394.40	2000.00
135	1 8 62 1	816.14	97871.34	1646.88	2306.07	285000.00	2266.49	145000.00	569.26	1067.26	3903.02
136	1 9 62 1	312.26	77544.36	653.86	906.07	225000.00	1914.39	115000.00	732.35	408.34	3055.08
137	1 10 62 1	814.84	44638.14	1350.00	2008.14	208715.50	2272.98	110541.68	661.46	1065.56	4000.00
138	1 11 62 1	2299.18	95000.00	1452.83	3309.86	290523.63	1935.05	147546.19	1058.30	3006.62	5999.97
139	1 12 62 1	1127.36	90599.12	1198.93	2109.49	225368.67	3169.12	115186.07	1356.62	1474.24	5999.99
140	1 1 63 1	409.50	63439.03	851.21	1181.96	144380.24	2499.09	74224.99	965.41	535.50	4000.00
141	1 2 63 1	474.24	36954.97	951.10	1334.14	81916.06	2458.85	42322.54	920.99	620.16	4000.00
142	1 3 63 1	377.78	0.00	978.79	1283.92	35000.00	2046.92	18000.00	671.63	494.02	3212.57
143	1 4 63 1	3356.60	80724.48	2000.00	4711.10	171529.77	2416.67	92915.30	1193.93	4389.40	8000.00
144	1 5 63 1	4113.20	196500.00	2230.32	5552.52	417643.58	1549.92	211869.35	1071.23	5378.80	7999.95
145	1 6 63 1	440.96	190812.84	536.53	892.69	332081.87	2330.59	166018.69	1092.77	576.64	4000.00
146	1 7 63 1	548.60	159726.21	1054.17	1497.27	345000.00	1287.18	175000.00	254.84	717.40	2259.41
147	1 8 63 1	546.00	114761.57	1277.27	1718.27	295230.84	2527.68	152505.65	758.32	714.00	4000.00
148	1 9 63 1	521.30	83618.93	1044.66	1465.71	236601.70	2450.99	123564.95	867.31	681.70	4000.00
149	1 10 63 1	456.04	51298.31	981.68	1350.02	170000.00	2433.17	85000.00	966.95	556.36	3996.49
150	1 11 63 1	4108.00	176734.85	2000.00	5318.00	471571.34	250.00	241144.32	377.95	5372.00	5999.95
151	1 12 63 1	1496.30	168996.48	1622.15	2830.70	467832.47	2891.51	237558.08	1151.77	1956.70	5999.98
152	1 1 64 1	520.78	16407.45	601.92	1022.55	308896.15	3607.36	155714.31	1711.61	681.02	5999.99
153	1 2 64 1	273.90	114913.80	1126.48	1346.98	165000.00	3848.59	85000.00	1428.85	357.00	5634.44
154	1 3 64 1	505.18	137245.20	142.00	550.03	65234.83	2172.53	35551.93	1166.85	660.62	4000.00
155	1 4 64 1	2730.00	180683.85	2000.00	4205.00	135288.07	3027.73	71222.54	1402.27	3570.00	8000.00
156	1 5 64 1	1495.52	149664.13	2000.00	3207.92	230370.62	1661.57	114887.56	382.75	1955.68	4000.00

LOC NO=

1.

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4.

PER DY MO YR DW

BRASSUA
INFLOWBRASSUA
EQP STORBRASSUA
OUTFLOWMOOSEHEAD
INFLOWMOOSEHEAD
EQP STORMOOSEHEAD
CUTFLOWFLAGGSTAF
EQP STORFLAGGSTAF
OUTFLOWBINGHAM 6
LOCAL IN

BI. FLOW RES

157	1	6	64	1	425.10	147615.38	459.53	802.88	215796.44	1047.80	109791.17	396.30	555.90	2000.00
158	1	7	64	1	687.96	128805.59	993.87	1549.53	254848.16	914.42	129270.81	185.94	899.64	2000.00
159	1	8	64	1	239.98	87015.35	919.62	1113.45	238396.59	1381.01	121289.50	305.17	313.82	2000.00
160	1	9	64	1	143.52	65907.02	498.25	614.17	194976.52	1343.86	99654.67	468.46	187.68	2000.00
161	1	10	64	1	263.12	38451.46	708.98	921.50	170000.00	1327.70	85000.00	430.61	344.08	2162.39
162	1	11	64	1	566.54	33940.82	643.01	1100.60	135000.00	1688.79	70000.00	666.09	740.86	3095.74
163	1	12	64	1	761.28	14906.69	1070.84	1685.72	110000.00	2092.30	55000.00	800.27	995.52	3888.08
164	1	1	65	1	514.80	0.00	757.23	1173.03	75000.00	1742.24	38000.00	652.67	673.20	3068.12
165	1	2	65	1	392.08	0.00	392.08	708.76	56864.14	1035.31	28811.16	451.97	512.72	2000.00
166	1	3	65	1	418.86	7000.00	305.02	643.33	35000.00	998.91	18000.00	481.91	547.74	2028.56
167	1	4	65	1	1594.06	15000.00	1459.62	2747.13	110000.00	1486.73	55000.00	543.09	2084.54	4114.36
168	1	5	65	1	1903.72	60000.28	1171.87	2709.49	216282.77	980.99	107581.75	529.53	2489.48	4000.00
169	1	6	65	1	646.36	90012.22	142.00	664.06	214195.40	699.14	108576.61	455.62	845.24	2000.00
170	1	7	65	1	223.08	94997.71	142.00	322.18	164516.34	1130.12	83450.32	578.16	291.72	2000.00
171	1	8	65	1	343.46	58859.96	931.18	1208.59	160629.79	1271.79	81723.93	279.07	449.14	2000.00
172	1	9	65	1	364.26	44454.42	606.35	900.56	146326.60	1140.93	74789.15	382.73	476.34	2000.00
173	1	10	65	1	1014.00	28148.47	1279.19	2098.19	170000.00	1713.18	85000.00	574.94	1326.00	3614.12
174	1	11	65	1	1062.10	32257.08	993.05	1850.90	167267.90	1896.82	88681.42	714.28	1388.90	4000.00
175	1	12	65	1	508.30	25788.16	613.51	1024.06	110000.00	1955.41	55000.00	919.22	664.70	3539.33
176	1	1	66	1	453.18	0.00	872.58	1238.61	75000.00	1807.82	38000.00	607.64	592.62	3008.08
177	1	2	66	1	187.72	2539.20	142.00	293.62	26205.69	1172.20	13277.55	582.32	245.48	2000.00
178	1	3	66	1	1382.16	2453.90	1383.55	2499.91	77576.82	1664.45	42510.58	528.11	1807.44	4000.00
179	1	4	66	1	2782.00	48986.81	2000.00	4247.00	152410.96	2989.39	82207.03	1372.61	3638.00	8000.00
180	1	5	66	1	2943.20	140000.00	1463.03	3840.23	345000.00	708.12	175000.00	641.69	3848.80	5198.51
181	1	6	66	1	947.44	187927.71	142.00	907.24	299441.44	1672.87	151447.07	1088.17	1238.96	4000.00
182	1	7	66	1	374.92	150479.83	983.94	1286.76	301228.66	1257.70	152797.15	252.02	490.28	2000.00
183	1	8	66	1	172.64	102450.45	953.75	1093.19	278310.16	1465.92	141596.40	308.32	225.76	2000.00
184	1	9	66	1	130.78	77116.87	556.52	662.15	225000.00	1558.04	115000.00	542.53	171.02	2271.59
185	1	10	66	1	537.94	44575.07	1067.17	1501.66	170000.00	2396.14	85000.00	881.01	703.46	3980.61
186	1	11	66	1	1612.78	45664.46	1594.47	2897.10	255000.00	1468.65	130000.00	422.33	2109.02	4000.00
187	1	12	66	1	836.94	62270.27	566.88	1242.87	211587.31	1948.90	108784.36	956.64	1094.46	4000.00
188	1	1	67	1	465.14	50754.78	652.42	1028.11	128889.66	2373.04	67046.43	1018.70	608.26	4000.00
189	1	2	67	1	272.48	10413.47	998.85	1218.93	75000.00	2189.25	38000.00	722.12	356.32	3267.59
190	1	3	67	1	233.74	7000.00	289.25	478.04	32170.04	1174.60	16544.59	519.74	305.66	2000.00
191	1	4	67	1	1896.18	15000.00	1761.74	3293.27	110000.00	1985.31	55000.00	739.41	2479.62	5204.35
192	1	5	67	1	3601.00	140600.00	1568.10	4476.60	345000.00	654.75	175000.00	679.92	4709.00	6043.56
193	1	6	67	1	1899.04	196500.00	949.54	2483.38	435000.00	970.90	220000.00	631.52	2483.36	4085.78
194	1	7	67	1	887.12	186097.63	1056.30	1772.82	416758.39	2069.48	212488.75	770.44	1160.08	4000.00
195	1	8	67	1	591.24	148854.23	1196.94	1674.48	371714.31	2407.04	188647.07	819.80	773.16	4000.00
196	1	9	67	1	715.52	125000.00	1116.40	1694.32	315000.00	2647.42	160000.00	1004.30	935.68	4587.40
197	1	10	67	1	956.02	95001.01	1443.90	2216.07	255000.00	3191.86	130000.00	1186.53	1250.18	5628.57
198	1	11	67	1	730.60	95001.28	730.60	1320.70	207182.04	2124.29	107006.75	920.31	955.40	4000.00
199	1	12	67	1	767.00	62816.11	1290.43	1909.93	185237.54	2266.82	96573.49	736.18	1003.00	4000.00
200	1	1	68	1	522.08	43094.24	842.82	1264.50	117388.89	2367.94	61658.92	949.34	682.72	4000.00
201	1	2	68	1	478.66	22155.97	842.67	1229.28	75000.00	1966.20	38000.00	761.10	625.94	3353.24
202	1	3	68	1	993.98	10277.05	1187.17	1990.00	73412.18	2015.82	40583.28	684.36	1299.82	4000.00
203	1	4	68	1	1235.40	143294.52	2000.00	5420.90	285000.00	1865.10	145000.00	1340.34	5538.60	8744.05
204	1	5	68	1	1361.36	145445.26	1326.38	2425.94	334457.02	1621.61	169392.03	598.15	1780.24	4000.00
205	1	6	68	1	1145.46	179167.97	582.74	1511.15	330061.29	1585.02	165116.65	911.84	1503.14	4000.00
206	1	7	68	1	509.86	156169.45	883.89	1295.70	342199.14	1098.30	173579.27	234.96	666.74	2000.00
207	1	8	68	1	16.38	113226.97	714.76	727.99	285000.00	1658.23	145000.00	476.76	21.42	2156.41
208	1	9	68	1	125.58	80778.99	670.88	772.31	225000.00	1780.63	115000.00	595.93	164.22	2540.78

LOC NO=

					1.	1.	1.	2.	2.	2.	3.	3.	4.	
PER	DY	MO	YR	DW	BRASSUA INFLOW	BRASSUA EOP STOR	BRASSUA OUTFLOW	MOOSEHEAD INFLOW	MOOSEHEAD EOP STOR	MOOSEHEAD OUTFLOW	FLAGGSTAF EOP STOR	FLAGGSTAF OUTFLOW	BINGHAM 6 LOCAL IN	BINGHAM 6 FLOW REG
209	1	10	68	1	89.44	45322.46	666.08	738.32	170000.00	1632.79	85000.00	553.26	116.96	2303.01
210	1	11	68	1	368.94	35155.81	539.79	837.78	135000.00	1425.97	70000.00	521.69	482.46	2430.12
211	1	12	68	1	509.08	15057.12	835.95	1247.13	110000.00	1653.71	55000.00	615.97	665.72	2935.40
212	1	1	69	1	407.16	0.00	652.04	980.90	75000.00	1550.11	38000.00	574.01	532.44	2656.56
213	1	2	69	1	393.12	0.00	393.12	710.64	57011.59	1034.53	28885.87	451.39	514.08	2000.30
214	1	3	69	1	329.94	7000.00	216.10	482.59	22419.39	1045.17	11529.97	523.37	431.46	2000.30
215	1	4	69	1	3411.20	90973.46	2000.00	4755.20	164810.47	2362.27	89831.04	1176.93	4460.80	8000.30
216	1	5	69	1	7763.60	196500.00	6047.40	12318.00	544000.00	6151.16	276000.00	2645.70	10152.40	18949.26
217	1	6	69	1	1702.48	196498.04	1702.51	3077.59	544000.00	3077.59	276000.00	1244.12	2226.32	6548.33
218	1	7	69	1	730.08	196500.00	730.05	1319.73	435000.00	3092.42	220000.00	1444.26	954.72	5491.40
219	1	8	69	1	780.52	150961.00	1391.02	2021.44	375000.00	2997.24	190000.00	1058.28	1020.68	5076.19
220	1	9	69	1	1225.38	126346.14	1773.48	2763.21	345555.16	3258.04	175477.72	1139.52	1602.42	5999.38
221	1	10	69	1	261.30	105776.33	595.83	806.88	235481.61	2597.03	121963.02	1061.27	341.70	4000.00
222	1	11	69	1	3289.00	182478.27	2000.00	4656.50	448632.32	1074.44	227821.17	624.52	4301.00	5999.96
223	1	12	69	1	2385.76	196500.00	2157.72	4084.68	544000.00	2533.70	276000.00	959.90	3119.84	6613.44
224	1	1	70	1	1037.14	196498.04	1037.17	1874.86	462200.39	3205.19	234149.04	1438.54	1356.26	5999.99
225	1	2	70	1	1526.46	171560.92	1975.47	3208.38	442173.34	3568.98	276000.00	361.93	1996.14	5927.06
226	1	3	70	1	583.44	196500.00	177.85	649.09	221699.23	4234.71	117607.69	3002.33	762.96	7999.39
227	1	4	70	1	3749.20	196500.00	3749.20	6777.40	399439.44	3790.42	202882.50	1306.73	4902.80	9999.35
228	1	5	70	1	4230.20	196500.00	4230.20	7646.90	544000.00	5295.88	276000.00	1902.18	5531.80	12729.86
229	1	6	70	1	743.34	196498.04	743.37	1343.76	425000.00	3175.54	220000.00	1484.31	972.06	5631.31
230	1	7	70	1	321.10	186097.44	490.25	749.60	345000.00	2213.29	175000.00	966.49	419.90	3599.68
231	1	8	70	1	44.72	123129.46	1068.78	1104.90	285000.00	2080.69	145000.00	520.58	58.48	2659.75
232	1	9	70	1	187.72	83169.25	859.26	1010.88	225000.00	2019.20	115000.00	641.34	245.48	2906.32
233	1	10	70	1	1252.82	90864.79	1137.67	2157.64	255000.00	1669.74	130000.00	678.88	1651.38	4000.30
234	1	11	70	1	754.52	93205.71	715.18	1324.60	209359.77	2091.60	107562.83	921.72	986.68	4000.00
235	1	12	70	1	626.08	62953.45	1118.08	1623.76	163284.86	2373.08	86400.30	808.20	818.72	4000.30
236	1	1	71	1	324.22	36617.81	752.52	1014.39	75000.00	2450.19	38000.00	1024.07	423.98	3898.24
237	1	2	71	1	511.94	0.00	1171.27	1584.76	75000.00	1584.76	38000.00	374.11	669.46	2628.33
238	1	3	71	1	463.32	0.00	463.32	837.54	35000.00	1488.07	18000.00	663.84	605.88	2757.79
239	1	4	71	1	2888.60	52876.14	2000.00	4333.10	122296.25	2866.06	62888.16	1356.54	3777.40	8000.30
240	1	5	71	1	5249.40	196500.00	2913.62	7153.52	524836.03	606.93	266273.56	528.40	6864.60	7999.33
241	1	6	71	1	530.40	195637.55	544.89	973.29	435000.00	2483.02	220000.00	1165.24	693.60	4341.96
242	1	7	71	1	186.16	186015.32	342.65	493.01	345000.00	1956.70	175000.00	867.88	243.44	3068.32
243	1	8	71	1	325.00	123100.02	1348.20	1610.70	285000.00	2586.50	145000.00	725.40	425.00	3736.89
244	1	9	71	1	134.68	83162.14	805.85	914.63	225000.00	1922.95	115000.00	602.58	176.12	2701.65
245	1	10	71	1	216.32	46308.59	815.68	990.40	170000.00	1884.87	85000.00	645.98	282.88	2813.73
246	1	11	71	1	229.84	27085.06	552.90	738.54	135000.00	1326.72	70000.00	420.04	300.56	2047.32
247	1	12	71	1	316.68	0.00	757.17	1012.95	110000.00	1419.53	55000.00	475.37	414.12	2309.02
248	1	1	72	1	256.10	0.00	256.10	462.95	68090.16	1144.54	34499.01	520.56	334.90	2000.30
249	1	2	72	1	289.38	7000.00	167.69	401.42	29580.27	1070.90	14587.34	550.68	378.42	2000.30
250	1	3	72	1	485.42	7000.00	485.42	877.49	24030.89	967.74	12358.74	397.48	634.78	2000.30
251	1	4	72	1	1264.90	15000.00	1130.46	2152.11	110000.00	707.37	55000.00	207.75	1654.10	2569.22
252	1	5	72	1	7194.20	196500.00	4242.43	10053.13	544000.00	2994.90	276000.00	1663.13	9407.80	14065.83
253	1	6	72	1	1713.40	196498.04	1713.43	3097.33	544000.00	3097.33	276000.00	1252.10	2240.60	6596.33
254	1	7	72	1	1409.72	196500.00	1409.69	2548.31	508458.82	3126.32	276000.00	1030.18	1843.48	5999.38
255	1	8	72	1	396.02	184260.09	505.08	752.25	375000.00	2922.72	190000.00	1622.27	400.18	4945.16
256	1	9	72	1	75.66	134939.42	904.51	965.62	257353.45	2942.71	136263.18	958.35	98.94	4000.30
257	1	10	72	1	335.14	77857.63	1262.82	1533.51	184481.55	2718.64	99481.55	843.10	438.26	4000.30
258	1	11	72	1	767.00	56976.10	1118.59	1738.09	158689.44	2171.54	83714.94	825.46	1003.00	4000.30
259	1	12	72	1	853.84	31685.67	1265.14	1954.78	145507.17	2169.17	78161.86	714.27	1116.56	4000.30
260	1	1	73	1	756.86	22057.44	913.45	1524.76	109230.75	2114.73	57105.54	895.53	989.74	4000.30

LOC NO=

PER	DY	MO	YR	DW	1. BRASSUA INFLOW	1. BRASSUA EOP STOR	1. BRASSUA OUTFLOW	2. MOOSEHEAD INFLOW	2. MOOSEHEAD EOP STOR	2. MOOSEHEAD OUTFLOW	3. FLAGGSTAF EOP STOR	3. FLAGGSTAF OUTFLOW	4. BINGHAM G LOCAL IN	4. BINGHAM G FLOW RES
261	1	2	73	1	998.40	18047.48	1070.60	1877.00	105371.13	1946.50	56089.03	747.90	1305.60	4000.00
262	1	3	73	1	1575.86	34333.54	1311.00	2583.81	135000.00	2101.95	75000.00	844.04	2060.74	5006.72
263	1	4	73	1	4898.49	196500.00	2173.14	6129.54	380538.83	2003.19	193322.73	1591.15	6405.60	9999.94
264	1	5	73	1	3582.80	196500.00	3582.80	6476.60	544000.00	3818.20	276000.00	1273.60	4685.20	9777.30
265	1	6	73	1	1478.10	196498.04	1478.13	2671.98	531619.61	2880.04	269639.43	1187.04	1932.90	5999.98
266	1	7	73	1	1513.46	195318.40	1532.64	2755.05	525128.77	2860.62	266304.69	1160.22	1979.14	5999.98
267	1	8	73	1	1019.72	189594.25	1112.81	1936.43	444180.86	3252.91	225204.46	1413.60	1333.48	5999.99
268	1	9	73	1	959.66	160249.74	1452.80	2227.91	372305.44	3435.80	189028.08	1309.25	1254.94	5999.99
269	1	10	73	1	988.78	126263.42	1541.51	2340.14	304980.67	3435.05	155249.75	1271.91	1293.02	5999.99
270	1	11	73	1	923.78	116118.23	1094.27	1840.40	255000.00	2680.34	130000.00	1099.40	1208.02	4987.76
271	1	12	73	1	3619.20	196500.00	2311.93	5235.13	525132.52	841.91	266477.54	425.24	4732.80	5999.95
272	1	1	74	1	895.96	190587.68	992.11	1715.77	425241.59	3340.32	215239.88	1488.03	1171.64	5999.99
273	1	2	74	1	475.54	158490.51	1053.47	1437.56	212166.05	5274.13	234539.90	0.00	621.86	5895.99
274	1	3	74	1	1177.28	196500.00	559.12	1510.00	135000.00	2764.97	75000.00	3454.95	1539.52	7759.44
275	1	4	74	1	4186.00	196500.00	4186.00	7567.00	379955.88	3450.44	193027.88	1075.50	5474.00	9999.95
276	1	5	74	1	5738.20	196500.00	5738.20	10372.90	544000.00	7705.02	276000.00	2843.91	7503.80	18052.72
277	1	6	74	1	1562.86	196458.04	1562.89	2825.20	544000.00	2825.20	276000.00	1142.09	2043.74	6011.33
278	1	7	74	1	1000.22	196500.00	1000.19	1808.06	456545.07	3230.36	231069.03	1461.65	1307.98	5999.99
279	1	8	74	1	406.90	166381.08	896.73	1225.38	375000.00	2551.56	190000.00	965.26	532.10	4048.93
280	1	9	74	1	282.62	128866.50	913.06	1141.33	282541.70	2695.12	146634.82	935.30	369.58	4000.00
281	1	10	74	1	166.40	84750.30	883.87	1018.27	175845.68	2753.49	90845.68	1028.91	217.60	4000.00
282	1	11	74	1	639.08	56262.26	1118.84	1635.02	135000.00	2321.44	70000.00	817.34	835.72	3974.50
283	1	12	74	1	1209.00	22747.17	1753.09	2729.59	182922.12	1950.22	95500.49	468.78	1581.00	4000.00
284	1	1	75	1	506.48	30511.39	380.21	789.29	95206.15	2215.83	49277.85	1121.85	662.32	4000.00
285	1	2	75	1	359.32	0.00	908.70	1198.92	75000.00	1562.74	38000.00	465.65	469.88	2498.27
286	1	3	75	1	901.94	6402.51	797.81	1526.30	49143.28	1963.08	25803.82	857.46	1179.46	4000.00
287	1	4	75	1	2186.86	17521.61	2000.00	3766.31	110000.00	2726.79	55000.00	1107.44	2859.74	6693.97
288	1	5	75	1	4245.80	155612.49	2000.00	5429.30	345000.00	1607.45	194111.75	840.30	5552.20	7999.94
289	1	6	75	1	1678.04	196500.00	990.91	2346.25	427982.31	951.71	216267.19	853.93	2194.36	4000.00
290	1	7	75	1	281.58	185427.89	461.65	689.08	345000.00	2038.64	175000.00	876.91	368.22	3283.76
291	1	8	75	1	69.42	122889.43	1086.50	1142.57	285000.00	2118.36	145000.00	538.63	90.78	2747.76
292	1	9	75	1	260.00	83111.31	928.48	1138.48	225000.00	2146.80	115000.00	694.16	340.00	3180.96
293	1	10	75	1	626.60	46287.56	1225.47	1731.57	182028.52	2430.43	97028.52	750.17	819.40	4000.00
294	1	11	75	1	825.50	41428.59	907.16	1573.91	153888.77	2046.80	80935.61	873.70	1079.50	4000.00
295	1	12	75	1	728.00	24250.77	1007.37	1595.37	117929.60	2180.18	60286.40	867.82	952.00	4000.00
296	1	1	76	1	520.00	2232.50	878.09	1298.09	75000.00	1996.26	38000.00	742.45	680.00	3418.71
297	1	2	76	1	889.20	6593.09	813.39	1531.59	75000.00	1531.59	38000.00	649.80	1162.80	3344.19
298	1	3	76	1	2111.20	36000.00	1730.53	3435.73	135000.00	2459.94	75000.00	941.06	2760.80	6161.80
299	1	4	76	1	4953.00	196500.00	2154.92	6155.42	385959.60	1937.96	196064.51	1584.97	6477.00	9999.94
300	1	5	76	1	2834.00	196500.00	2834.00	5123.00	504427.55	3196.33	255915.49	1097.63	3706.00	7999.96
301	1	6	76	1	569.40	194718.97	599.33	1059.23	434621.40	2232.34	219798.62	1023.06	744.60	4000.00
302	1	7	76	1	2012.40	195481.42	2000.00	3625.40	504792.48	2484.19	255856.69	884.18	2631.60	5999.97
303	1	8	76	1	1840.80	185692.46	2000.00	3486.80	544000.00	2849.16	276000.00	1017.61	2407.20	6273.97
304	1	9	76	1	465.40	196500.00	283.78	659.68	370541.97	3574.69	188134.80	1816.70	608.60	5999.99
305	1	10	76	1	1749.80	181115.58	2000.00	3413.30	410428.32	2764.62	208520.88	947.16	2288.20	5999.98
306	1	11	76	1	1068.60	157783.87	1460.70	2323.80	351211.95	3318.95	178605.34	1283.64	1397.40	5999.99
307	1	12	76	1	938.60	127435.26	1432.17	2190.27	273653.58	3451.61	139555.57	1320.97	1227.40	5999.99
308	1	1	77	1	280.80	90118.76	887.69	1114.49	180169.13	2634.84	90810.09	997.96	367.20	4000.00
309	1	2	77	1	208.00	53138.15	873.86	1041.86	85608.14	2744.50	44630.09	983.50	272.00	4000.00
310	1	3	77	1	5344.00	196500.00	4012.48	9136.48	544000.00	1681.56	276000.00	873.18	8296.00	10850.74
311	1	4	77	1	3692.00	196500.00	3692.00	6674.00	544000.00	6674.00	276000.00	2698.00	4828.00	14200.00
312	1	5	77	1	912.60	196498.04	912.63	1649.73	360866.49	4628.07	183052.84	2178.52	1193.40	7999.99

LOC NO=					1.	1.	1.	2.	2.	2.	3.	3.	4.	4.
PER	DY	MO	YR	OW	BRASSUA INFLOW	BRASSUA EOP STOR	BRASSUA OUTFLOW	MOOSEHEAD INFLOW	MOOSEHEAD EOP STOR	MOOSEHEAD OUTFLOW	FLAGGSTAF EGP STOR	FLAGGSTAF OUTFLOW	BINGHAM 6 LOCAL IN	BINGHAM 3 FLOW REG
313	1	6	77	1	1768.00	188257.23	1906.49	3334.49	435000.00	2088.65	220000.00	671.09	2312.00	5071.74
314	1	7	77	1	392.60	185310.97	440.52	757.62	345000.00	2221.30	175000.00	1018.74	513.40	3753.45
315	1	8	77	1	626.60	122847.52	1642.46	2148.56	318118.52	2585.73	166578.21	594.87	819.40	4000.00
316	1	9	77	1	1053.00	125000.00	1016.83	1867.33	315000.00	1919.73	160000.00	880.05	1377.00	4176.78
317	1	10	77	1	4264.00	196500.00	3101.18	6545.18	544000.00	2820.91	276000.00	1229.47	5576.00	9626.38
318	1	11	77	1	1791.40	196498.04	1791.43	3238.33	544000.00	3238.33	276000.00	1309.10	2342.60	6890.03
319	1	12	77	1	889.20	196500.00	889.17	1607.37	438569.45	3322.01	222788.97	1515.18	1162.80	5999.99
320	1	1	78	1	2652.00	196500.00	2652.00	4794.00	544000.00	3079.36	276000.00	1072.62	3468.00	7619.98
321	1	2	78	1	842.40	196498.04	842.44	1522.84	390717.70	4282.79	276000.00	615.60	1101.60	5999.99
322	1	3	78	1	728.00	196500.00	727.97	1315.97	226841.36	3981.12	120134.75	3066.87	952.00	7999.99
323	1	4	78	1	3900.00	196500.00	3900.00	7050.00	427452.76	3678.66	217051.39	1221.29	5100.00	9999.95
324	1	5	78	1	3536.00	196500.00	3536.00	6392.00	544000.00	4496.57	276000.00	1625.31	4624.00	10745.88
325	1	6	78	1	1040.00	196498.04	1040.03	1880.03	465383.11	3201.21	235609.67	1438.77	1360.00	5999.99
326	1	7	78	1	309.40	188997.07	431.39	681.29	353862.65	2494.97	181848.41	1100.43	404.60	4000.00
327	1	8	78	1	158.60	127346.13	1161.24	1289.34	285000.00	2489.27	145000.00	715.17	207.40	3331.94
328	1	9	78	1	106.60	84187.07	831.90	918.00	225000.00	1926.32	115000.00	582.06	139.40	2647.78
329	1	10	78	1	157.30	46732.70	766.43	893.48	170000.00	1787.95	85000.00	602.85	205.70	2596.50
330	1	11	78	1	150.80	12856.66	720.10	841.90	134591.01	1436.96	69787.93	365.84	197.20	2000.00
331	1	12	78	1	96.20	0.00	305.29	382.99	78006.23	1303.24	39003.11	570.96	125.80	2000.00
332	1	1	79	1	540.80	0.00	540.80	977.60	75000.00	1026.49	38000.00	411.51	707.20	2145.20
333	1	2	79	1	327.60	0.00	327.60	592.20	47722.49	1083.35	24179.39	488.25	428.40	2000.00
334	1	3	79	1	3120.00	68867.12	2000.00	4520.00	161143.33	2675.41	87847.94	1244.55	4080.00	7999.96
335	1	4	79	1	4524.00	196500.00	2379.09	6033.09	372461.58	2481.82	189237.33	1602.12	5916.00	9999.94
336	1	5	79	1	3068.00	196500.00	3068.00	5546.00	527653.93	3022.08	267703.75	965.88	4012.00	7999.96
337	1	6	79	1	1274.00	195764.38	1286.36	2315.36	484967.44	3032.72	245671.35	1301.26	1666.00	5999.98
338	1	7	79	1	361.40	150756.10	442.20	734.10	378419.81	2466.91	196702.27	1060.49	472.60	4000.00
339	1	8	79	1	249.60	136794.57	1127.84	1329.44	291881.24	2736.83	150217.33	936.77	326.40	4000.00
340	1	9	79	1	345.80	88676.43	1154.44	1433.74	225000.00	2557.70	115000.00	846.22	452.20	3856.12
341	1	10	79	1	878.80	48590.37	1530.73	2240.53	224515.59	2248.41	117447.60	602.39	1149.20	4000.00
342	1	11	79	1	1097.20	61631.12	878.05	1764.25	226107.46	1737.49	115506.08	827.71	1434.80	4000.00
343	1	12	79	1	676.00	57625.03	741.45	1287.15	170289.41	2194.93	89446.31	921.07	884.00	4000.00
344	1	1	80	1	286.00	37115.42	619.55	850.55	75000.00	2400.26	38000.00	1048.93	374.00	3823.20
345	1	2	80	1	130.00	7000.00	653.55	758.55	37721.13	1406.64	19112.04	423.36	170.00	2000.00
346	1	3	80	1	577.20	7000.00	577.20	1043.40	35000.00	1087.65	18000.00	439.89	754.80	2282.34
347	1	4	80	1	2990.00	65909.95	2000.00	4415.00	132758.05	2772.15	69599.50	1317.85	3910.00	8000.00
348	1	5	80	1	1287.00	85784.08	963.78	2003.28	200000.00	909.71	100000.00	446.09	1683.00	3038.80
349	1	6	80	1	356.20	98530.05	142.00	429.70	165542.50	1008.77	84223.38	525.43	465.80	2000.00
350	1	7	80	1	273.00	76809.30	626.25	846.75	141365.44	1239.95	71707.11	403.05	357.00	2000.00
351	1	8	80	1	260.00	28421.21	1046.95	1256.95	132539.67	1400.48	67432.47	259.52	340.00	2000.00
352	1	9	80	1	213.20	0.00	690.83	863.03	104676.26	1331.28	53501.20	389.92	278.80	2000.00
353	1	10	80	1	642.20	0.00	642.20	1160.90	124718.03	834.96	62359.02	325.24	839.80	2000.00
354	1	11	80	1	704.60	20303.29	363.40	932.50	135000.00	759.71	70000.00	386.49	921.40	2067.50
355	1	12	80	1	709.80	13703.38	817.14	1390.44	110000.00	1797.02	55000.00	762.65	928.20	3487.86
356	1	1	81	1	215.80	0.00	438.66	612.96	70859.63	1249.51	35902.21	468.29	282.20	2000.00
357	1	2	81	1	2207.40	50000.00	1307.12	3090.02	165000.00	1394.95	85000.00	729.06	2886.60	5010.61
358	1	3	81	1	670.80	82515.12	142.00	683.80	83789.08	2004.55	46382.13	1118.25	877.20	4060.00
359	1	4	81	1	1313.00	41635.18	2000.00	3060.50	110000.00	2620.02	55000.00	814.67	1717.00	5151.59
360	1	5	81	1	1222.00	69322.59	771.71	1758.71	200000.00	295.03	100000.00	161.16	1598.00	2054.18
361	1	6	81	1	959.40	112714.40	230.19	1005.09	236730.04	387.83	120441.60	357.57	1254.60	2000.00
362	1	7	81	1	460.20	123855.13	279.02	650.72	220195.30	919.62	111693.27	478.58	601.80	2000.00
363	1	8	81	1	520.00	78033.15	1265.21	1685.21	250343.03	1194.91	127367.51	125.09	680.00	2000.00
364	1	9	81	1	998.40	66507.37	1192.09	1998.49	247506.83	2046.16	132208.69	648.24	1305.60	4000.00

LOC NO=

C NO=						1.	1.	1.	2.	2.	2.	3.	3.	4.	
PER	DY	MO	YR	DW		BRASSUA INFLOW	BRASSUA EOP STOR	BRASSUA OUTFLOW	MOOSEHEAD INFLOW	MOOSEHEAD EOP STOR	MOOSEHEAD OUTFLOW	FLAGGSTAF EOP STOR	FLAGGSTAF OUTFLOW	BINGHAM 6 LOCAL IN	BINGHAM 6 FLOW RES
365	1	10	81	1		1729.00	95000.00	1265.62	2662.12	259113.64	2473.35	132078.17	1265.62	2261.00	5999.98
366	1	11	81	1		1302.60	96070.24	1284.61	2336.71	255000.00	2405.85	130000.00	986.82	1703.40	5096.37
367	1	12	81	1		665.60	80320.46	921.74	1459.34	206007.67	2256.11	106198.68	873.49	870.40	4000.00
368	1	1	82	1		603.20	54456.98	1023.82	1511.02	155425.58	2333.65	79343.56	877.55	788.80	4000.00
369	1	2	82	1		405.60	37470.79	711.45	1039.05	76995.45	2451.24	39247.16	1018.36	530.40	4000.00
370	1	3	82	1		574.60	0.00	1184.00	1648.10	35000.00	2331.08	18000.00	765.45	751.40	3847.92
371	1	4	82	1		4342.00	139360.71	2000.00	5507.00	285000.00	1305.67	145000.00	1038.73	5678.00	8022.40
372	1	5	82	1		1887.60	196500.00	958.33	2482.93	345000.00	1507.14	175000.00	891.50	2468.40	4867.04
373	1	6	82	1		678.60	187543.17	829.12	1377.22	296231.03	2196.80	150013.85	915.80	887.40	4000.00
374	1	7	82	1		214.50	149544.16	832.49	1005.74	273342.77	1377.97	138652.13	341.53	280.50	2000.00
375	1	8	82	1		267.80	95913.60	1140.00	1356.30	269080.84	1425.62	136500.78	224.18	350.20	2000.00
376	1	9	82	1		252.20	73923.72	621.75	825.45	225000.00	1566.24	115000.00	552.35	329.80	2448.39
377	1	10	82	1		227.50	44103.95	712.47	896.22	170000.00	1790.69	85000.00	654.15	297.50	2742.34
378	1	11	82	1		1170.00	34854.48	1325.44	2270.44	193153.91	1881.33	100648.06	588.67	1530.00	4000.00
379	1	12	82	1		587.60	36159.50	566.38	1040.98	122424.18	2191.27	63282.79	1040.33	768.40	4000.00
380	1	1	83	1		803.40	16687.75	1120.07	1768.97	98248.35	2162.15	50975.82	787.25	1050.60	4000.00
381	1	2	83	1		1703.00	50900.00	1103.19	2478.69	165000.00	1276.78	85000.00	631.87	2227.00	4135.65
382	1	3	83	1		2563.60	196500.00	181.04	2251.64	140277.22	2653.71	77593.45	1993.85	3352.40	7999.97
383	1	4	83	1		5512.00	196500.00	5512.00	9964.00	544000.00	3179.31	276000.00	693.72	7208.00	11081.03
384	1	5	83	1		2782.00	196500.00	2782.00	5029.00	544000.00	5029.00	276000.00	2033.00	3638.00	10700.00
385	1	6	83	1		1066.00	196498.04	1066.03	1927.03	469314.06	3182.15	237629.24	1423.83	1394.00	5999.99
386	1	7	83	1		509.60	189372.22	625.49	1037.09	387989.73	2359.68	200642.83	973.92	666.40	4000.00
387	1	8	83	1		291.20	139714.85	1098.79	1333.99	302601.72	2722.67	158601.33	896.53	380.80	4000.00
388	1	9	83	1		241.80	93566.51	1017.34	1212.64	225000.00	2516.76	115000.00	909.43	316.20	3742.39
389	1	10	83	1		299.00	50613.85	997.55	1239.05	170000.00	2133.52	85000.00	706.40	391.00	3230.92
390	1	11	83	1		2834.00	100241.02	2000.00	4289.00	329375.67	1610.64	167573.87	683.32	3706.00	5959.96
391	1	12	83	1		2493.40	196500.00	927.92	2941.82	412037.86	1597.47	209398.42	1141.90	3260.60	5999.97
392	1	1	84	1		540.80	155140.10	1213.44	1650.24	280550.04	3788.66	141211.65	1504.14	707.20	5999.99
393	1	2	84	1		746.20	103567.76	1642.77	2245.47	165000.00	4254.29	128292.29	769.90	975.80	5999.99
394	1	3	84	1		1326.00	176370.15	142.00	1213.00	135000.00	1700.90	75000.00	1835.70	1734.00	5270.60
395	1	4	84	1		5746.00	196500.00	5407.71	10048.71	544000.00	3175.34	276000.00	821.13	7514.00	11510.47
396	1	5	84	1		3510.00	196500.00	3510.00	6345.00	544000.00	6345.00	276000.00	2565.00	4590.00	13500.00
397	1	6	84	1		3016.00	196500.00	3016.00	5452.00	544000.00	5452.00	276000.00	2204.00	3944.00	11600.00
398	1	7	84	1		1047.80	196498.04	1047.83	1894.13	463981.09	3195.50	234889.37	1434.29	1370.20	5999.99
399	1	8	84	1		244.40	168941.36	692.56	889.96	356067.90	2644.97	182204.43	1035.43	319.60	4000.00
400	1	9	84	1		130.00	123211.06	898.51	1003.51	245158.28	2867.38	130576.85	962.62	170.00	4000.00
401	1	10	84	1		179.40	69321.27	1055.82	1200.72	170000.00	2423.03	85000.00	872.33	234.60	3529.96
402	1	11	84	1		397.80	46741.44	777.26	1098.56	125000.00	1686.75	70000.00	542.78	520.20	2749.73
403	1	12	84	1		475.80	19290.33	922.24	1306.54	110000.00	1713.12	55000.00	591.65	622.20	2926.97
404	1	1	85	1		392.60	0.00	706.32	1023.42	75000.00	1592.63	38000.00	563.37	513.40	2669.41
405	1	2	85	1		829.40	2128.53	791.07	1460.97	75000.00	1460.97	38000.00	606.10	1084.60	3151.67
406	1	3	85	1		1414.40	6584.21	1341.94	2484.34	126716.67	1643.26	70371.08	507.14	1849.60	4000.00
407	1	4	85	1		2511.60	49148.82	1796.29	3824.89	163892.00	3200.15	89469.44	1515.45	3284.40	8000.00
408	1	5	85	1		1196.00	90200.91	528.36	1494.36	200000.00	907.13	100000.00	701.76	1564.00	3172.89
409	1	6	85	1		652.60	118792.90	172.10	699.20	200000.78	699.19	101754.78	447.41	853.40	2000.00
410	1	7	85	1		455.00	112991.56	549.35	916.85	193853.36	1016.83	98331.41	388.17	595.00	2000.00
411	1	8	85	1		187.20	65594.79	892.97	1044.17	170255.19	1427.95	86621.06	327.25	244.80	2000.00
412	1	9	85	1		481.00	48578.01	834.19	1222.69	177993.06	1092.66	90574.23	278.34	629.00	2000.00

SUM = 504552.8842420241.32 506779.37 914302.85***** 920828.8553577303.95 371350.73 659799.92 1951979.50

MAX = 7763.60 196500.00 6047.40 12318.00 544000.00 7705.02 276000.00 3454.95 10152.40 18949.26

MIN = 16.38 0.00 142.00 173.92 22229.46 250.00 11432.29 0.00 21.42 2000.00

PHAX= 216.00 24.00 216.00 216.00 37.00 276.00 37.00 274.00 216.00 216.00

AVG = 1224.64 102961.75 1230.05 2219.18 252281.53 2235.02 130042.00 901.34 1601.46 4737.91